

Earth Science Applications of Space Based Geodesy

DES-7355

Tu-Th

9:40-11:05

Seminar Room in 3892 Central Ave. (Long building)

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http://www.ceri.memphis.edu/people/smalley/ESCI7355/ESCI_7355_Applications_of_Space_Based_Geodesy.html

Class 10

One thing to keep in mind about the
phase velocity

is that it is an entirely mathematical construct.

Pure sine waves do not exist,
as a monochromatic wave train is infinitely long.

They are merely a tool to construct wave packets,
which have a group velocity,
and that is what we are measuring in experiments.

In fact, it may very well be that the phase velocity comes
out
higher than c ,
(e.g. in wave guides!)

This puzzles people, and some use that fact to claim that
the theory of relativity is wrong.

However, even if you had a pure sine wave, you couldn't
use it to transmit any information,

because it is unmodulated,
so there is no contradiction.

But it turns out that
even the group velocity may be higher than c ,
namely in the case of anomalous dispersion

Now how do we get around this?

Well, this kind of dispersion is so bad that the definition of our wave packet loses its meaning because it just disintegrates, and again we cannot use it to transmit information.

The only way would be to switch the signal on and off - these discontinuities propagate with the wavefront velocity

$$v_F = \lim_{k \rightarrow \infty} (\omega(k) / k)$$

And again, relativity is saved!

In terms of our GPS signals we get
(we are now mixing – multiplying, not adding.
G= GPS signal, R= Reference signal.)

$$R(t) \otimes G(t) = G_0 \sin(2\pi\phi_G(t)) \times R_0 \sin(2\pi\phi_R(t))$$

$$R(t) \otimes G(t) = \frac{G_0 R_0}{2} \left(\cos(2\pi(\phi_R(t) - \phi_G(t))) \cos(2\pi(\phi_R(t) + \phi_G(t))) \right)$$

Note this is in terms of phase, $\phi(t)$, not frequency
 (“usual” presentation; ωt , produces phase)

“Filter” to remove high frequency part

$$(\phi_R(t) + \phi_G(t))$$

leaving beat signal

$$B(t) = \frac{G_0 R_0}{2} \cos(2\pi(\phi_R(t) - \phi_G(t)))$$

$$B(t) = \frac{G_0 R_0}{2} \cos(2\pi\phi_B(t))$$

if you differentiate ϕ_B
you find the
beat frequency
the difference between the two frequencies
(actually one wants to take the absolute value)
– as we found before

$$\frac{d\phi_B(t)}{dt} = \frac{d\phi_R(t)}{dt} - \frac{d\phi_G(t)}{dt}$$
$$f_B = f_R - f_G$$

If the receiver copy of the signal has the same code applied as the satellite signal -

This discussion continues to hold (the -1's cancel)

(one might also worry about the Doppler shift effect on the codes, but this effect is second order)

If the receiver copy of the signal does not have the code applied (e.g. - we don't know the P code)

then this discussion will not work (at least not simply)

There are essentially two means by which the carrier wave can be recovered from the incoming modulated signal:

Reconstruct the carrier wave by removing the ranging code and broadcast message modulations.

Squaring, or otherwise processing the received signal without using a knowledge of the ranging codes.

To reconstruct the signal, the ranging codes (C/A and/or P code)

must be known.

The extraction of the Navigation Message can then be easily performed by reversing the process by which the bi-phase shift key modulation was carried out in the satellite.

In the squaring method no knowledge of the ranging codes is required.

The squaring removes the effects of the -1's
(but halves the wavelength and makes the signal noisier)

More complex signal processing is required to make carrier phase measurements on the L2 signal under conditions of Anti-Spoofing (don't know P-code).

As mentioned earlier:
can arbitrarily add $N(2\pi)$ to phase
and get same beat signal

This is because we have no direct measure of the
“total” (beat) phase

$$\Phi + N = \phi_R - \phi_G$$

(argument is $2\pi\phi$, so no 2π here)

$$\Phi + N = \phi_R - \phi_G$$

GPS receiver records Φ

total number of (beat) cycles since lock on satellite
N is fixed (as long as lock on satellite is maintained)

N is called the “ambiguity” (or “integer ambiguity”)

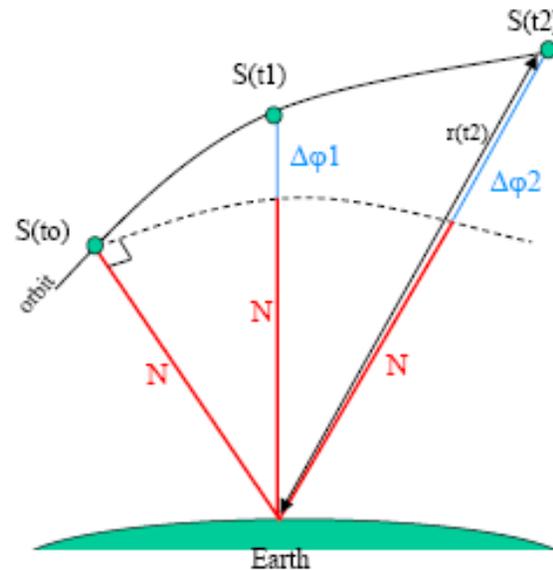
It is an integer (theoretically)

If loose lock – cycle slip, have to estimate new N.

Making a few reasonable assumptions we can interpret N geometrically to be the number of carrier wavelengths between the receiver (when it makes the first observation) and the satellite (when it transmitted the signal)

Phase measurements

- When a satellite is locked (at t_0), the GPS receiver starts tracking the incoming phase
- It counts the (real) number of phases as a function of time = $\Delta\phi(t)$
- But the initial number of phases N at t_0 is unknown...
- However, if no loss of lock, N is constant over an orbit arc



How to use (beat) phase to measure distance?

phase \rightarrow clock time \rightarrow distance

Phase to velocity and position

Consider a fixed transmitter and a fixed receiver

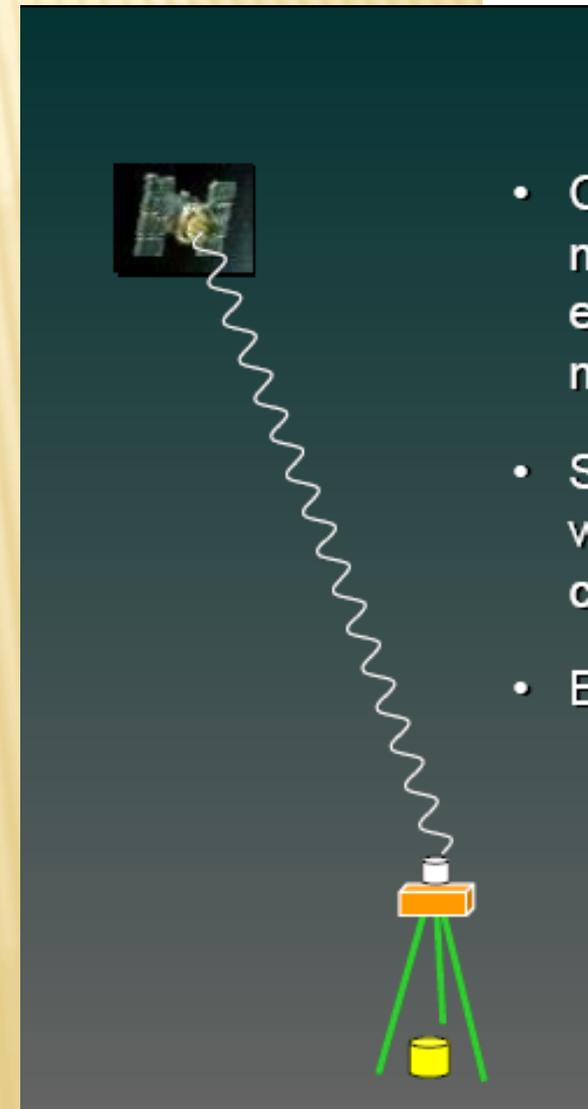
Receiver sees constant rate of change of phase (fixed frequency) equal to that of the transmitter

$$\Phi(t) = \phi_0 t + (N)$$

Integrated phase increases linearly with time



<http://www.npwrc.usgs.gov/perm/cranemov/location.htm>
<http://electron9.phys.utk.edu/phys135d/modules/m10/doppler.htm>

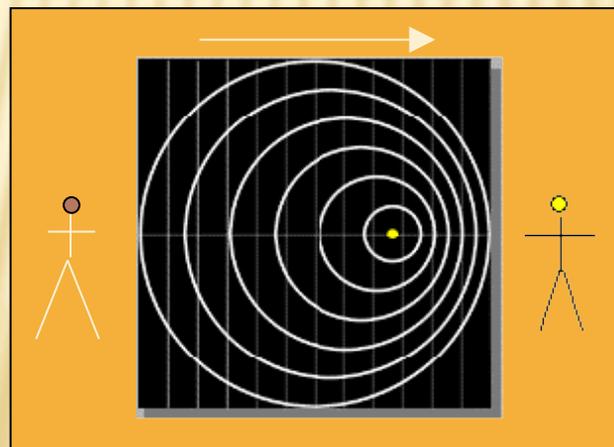


Next consider a transmitter moving on a line through a fixed receiver

Receiver again sees a constant rate of change of phase (frequency) – but it is no longer equal to that of the transmitter

$$\Phi(t) = \phi't + (N)$$

See lower frequency when XTR moving away

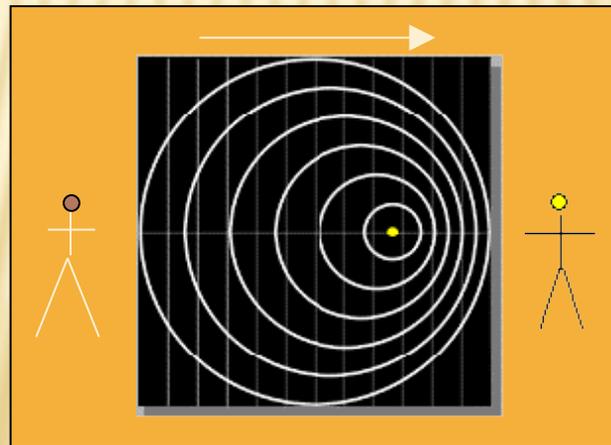


See higher frequency when XTR moving towards

The change in the rate of phase change (fixed change in frequency) observed at receiver, with respect to stationary transmitter, is proportional to velocity of moving transmitter.

$$f(\vec{x}, t) = f_0 - \frac{f_0}{c} v$$

c is speed of waves in medium,
 v is velocity of transmitter



(this is classical,
not relativistic)

If you knew the frequency transmitted by the moving transmitter.

You can use the
beat frequency

produced by combining the received signal with a receiver generated signal that is at the transmitted frequency

to determine the speed.

But we can do more.

We can

count the (beat) cycles
or measure the (beat) phase

of the beat signal as a function of time.

This will give us the change in distance.
(as will velocity times time)

So we can write

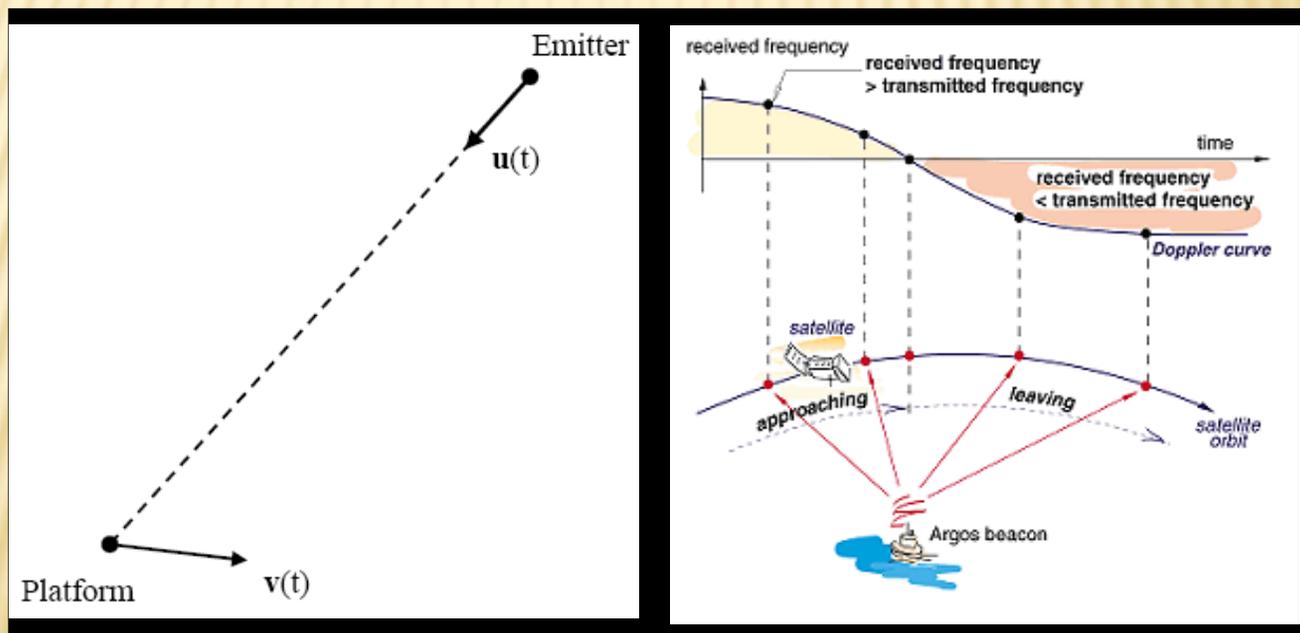
Beat phase (t) = change in distance to transmitter +
constant

Beat phase (at t = t_{fixed}) = distance to transmitter +
constant

Note the arbitrary constant –
can redo measurements from another position
(along trajectory of moving transmitter)
and get same result
(initial phase measurement will be different, but that will
not change the frequency or distance estimation)

Next – move the receiver off the path of the transmitter (and can also let the transmitter path be arbitrary, now have to deal with vectors.)

$$f(\vec{x}, t) = f_0 - \frac{f_0}{c} \vec{v}(t) \cdot \vec{u}(t)$$



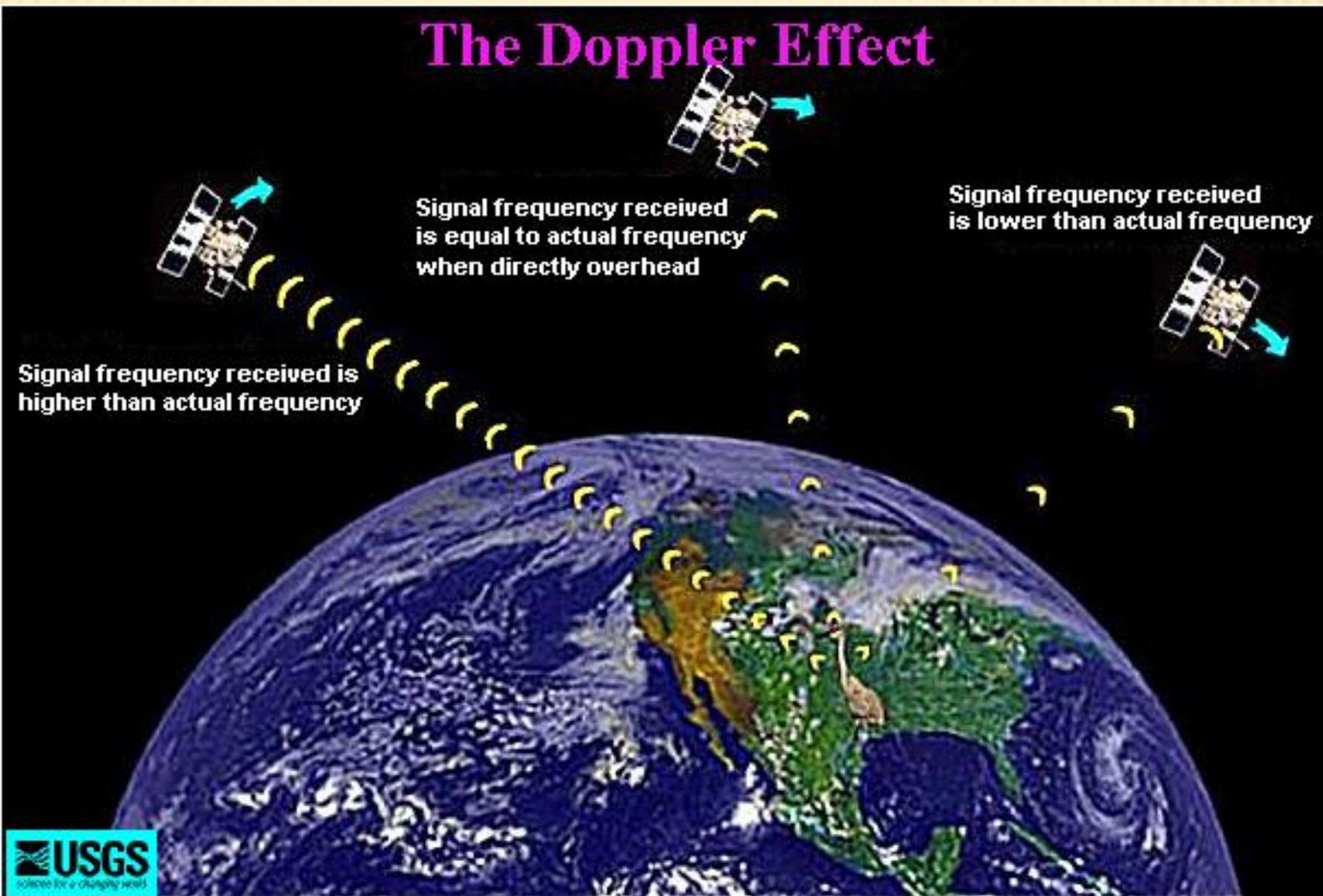
Can solve this for

Location of stationary transmitter from a moving receiver
(if you know \underline{x} and \underline{v} of receiver – how SARSAT, ELT,
EPIRB's [Emergency Position Indicating Radio Beacon]
work [or used to work – now also transmit location from GPS])

Location of moving transmitter
(solve for \underline{x} and \underline{v} of transmitter)
from a stationary receiver
(if you know \underline{x} of receiver)

(Doppler shift, change in frequency, more useful for
estimating velocity than position.
Integrate Doppler phase to get position.)

The Doppler Effect



Apply this to GPS
So far we have

Satellite carrier signal
Mixed with copy in receiver
After “low pass filter” – left with beat signal

Phase of beat signal equals reference phase minus
received phase plus unknown integer number full cycles

From here on we will follow convention and call

- Carrier beat phase -

-Carrier phase -

(remember it is NOT the phase of the incoming signal)

Consider the observation of satellite S

We can write the observed carrier (beat) phase as

$$\Phi^S(T) = \phi(T) - \phi^S(T) - N^S$$

Receiver replica of
signal

Incoming signal received from satellite S

Receiver clock time

Now assume that the phase from the satellite received at time T is equal to what it was when it was transmitted from the satellite

(we will eventually need to be able to model the travel time)

$$\phi^S(x, y, z, T) = \phi_{transmit}^S(x^S, y^S, z^S, T^S)$$

$$\Phi^S(T) = \phi(T) - \phi^S(T) - N^S$$

Use from before for receiver time $T(t) = \frac{(\phi(t) - \phi_0)}{f_0}$

$$\phi(T) = f_0 T + \phi_0$$

$$\phi_{transmit}^S(T^S) = f_0 T_{transmit}^S + \phi_0^S$$

So the carrier phase observable becomes

$$\Phi^S(T) = f_0 T + \phi_0 - f_0 T_{transmit}^S - \phi_0^S - N^S$$

$$\Phi^S(T) = f_0 (T - T_{transmit}^S) + \phi_0 - \phi_0^S - N^S$$

$$\Phi^S(T) = f_0(T - T_{transmit}^S) + \phi_0 - \phi_0^S - N^S$$

Terms with S are for each satellite
All other terms are equal for all observed satellites

(receiver ϕ_0 should be same for all satellites – no interchannel bias, and receiver should sample all satellites at same time – or interpolate measurements to same time)

T^S and N^S will be different for each satellite
Last three terms cannot be separated (and will not be an integer) – call them “carrier phase bias”

Now we will convert carrier phase to range

(and let the superscript $S \rightarrow$ satellite number, j ,
to handle more than one satellite, and

add a subscript for multiple receivers, A ,
to handle more than one receiver.)

$$\Phi_A^j(T_A) = f_0(T_{A, \text{received}} - T^{j, \text{transmitted}}) + \phi_{0_A} - \phi_0^j - N_A^j$$

We will also drop the “received” and “transmitted” reminders.

Times with superscripts will be for the transmission time by the satellite.

Times with subscripts will be for the reception time by the receiver.

$$\Phi_A^j(T_A) = f_0(T_A - T^j) + \phi_{0_A} - \phi_0^j - N_A^j$$

If we are using multiple receivers, they should all sample
at

exactly the same time
(same value for receiver clock time).

Values of clock times of sample – epoch.

With multiple receivers the clocks are not perfectly
synchronized, so the true measurement times will vary
slightly.

Also note – each receiver-satellite pair has its own
carrier phase ambiguity.

carrier phase to range
Multiply phase (in cycles, not radians) by wavelength to
get “distance”

$$L_A^j(T_A) = \lambda_0 \Phi_A^j(T_A)$$

$$L_A^j(T_A) = \lambda_0 \left(f_0 (T_A - T^j) + \phi_{0_A} - \phi_0^j - N_A^j \right)$$

$$L_A^j(T_k) = c (T_A - T^j) + \lambda_0 \left(\phi_{0_A} - \phi_0^j - N_A^j \right)$$

$$L_A^j(T_A) = c (T_A - T^j) + B_A^j$$

$L_A^j(T_A)$ is in units of meters

B_A^j is “carrier phase bias” (in meters)
(is not an integer)

$$L_A^j(T_A) = c (T_A - T^j) + B_A^j$$

a distance

This equation looks exactly like the equation for pseudo-range

$$P_R^S = \rho_R^S(t_R, t^S) + (\tau_R - \tau^S) c = \rho_R^S(t_R, t^S) + c \delta t$$

That we saw before

pseudo-range

constant

$$L_A^j(T_A) = c(T_A - T^j) + B_A^j$$

This equation also holds for both

L1 and L2

Clock biases same, but ambiguity different
(different wavelengths)

Now that we have things expressed as “distance” (range)

Follow pseudo range development

$$L_A^j(T_A) = c(T_A - T^j) + B_A^j$$

$$L_A^j(T_A) = \rho_A^j(t_A, t^j) + c\tau_A - c\tau^j + Z_A^j - I_A^j + B_A^j$$

Added a few things related to propagation of waves
Delay in signal due to

$$\begin{aligned} \text{Troposphere} &\sim Z_A^j \\ \text{Ionosphere} &\sim -I_A^j \end{aligned}$$

(ionospheric term has “-” since phase velocity increases)

Can include these effects in pseudo range development
also

$$P_A^j(T_k) = c (T_A - T^j)$$

$$P_A^j(T_A) = \rho_A^j(t_A, t^j) + c\tau_A - c\tau^j + Z_A^j + I_A^j$$

Delay in signal due to

$$\begin{array}{l} \text{Troposphere} + Z_A^j \\ \text{Ionosphere} + -I_A^j \end{array}$$

(ionospheric term now has “+” since group velocity to first order is same magnitude but opposite sign as phase velocity)

Now we have to fix the time

So far our expression has receiver and satellite clock time

-Not true time

Remember that the true time is the clock time adjusted by the clock bias

$$t_A = T_A - \tau_A$$

We know T_A exactly

(it is the receiver clock time which is written into the observation file – called a “time tag”)

$$t_A = T_A - \tau_A$$

But we don't know τ_A

(we need it to an accuracy of $1 \mu\text{sec}$)

How to estimate τ_A

- Use estimate of τ_A from pseudo range point positioning (if have receiver that uses the codes)
 - LS iteration of code and phase data simultaneously
 - If know satellite position and receiver location well enough (300 m for receiver – 1 μ sec of distance) can estimate it
- (this is how GPS is used for time transfer, once initialized can get time with only one satellite visible [if don't loose lock.])
- Modeling shortcut – linearize (Taylor series)

Eliminating clock biases using differencing

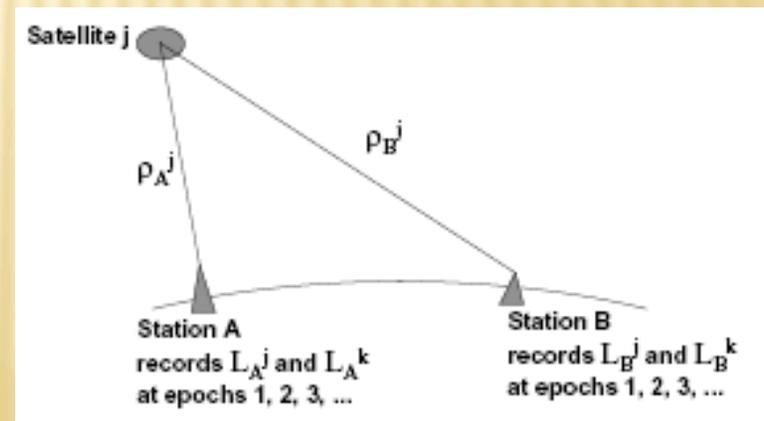
Return to our model for the phase observable

$$L_A^j(T_A) = \rho_A^j(t_A, t^j) + c\tau_A - c\tau^j + Z_A^j - I_A^j + B_A^j$$

clock error - receiver

clock error - satellite

What do we get if we combine measurements made by two receivers at the same epoch?



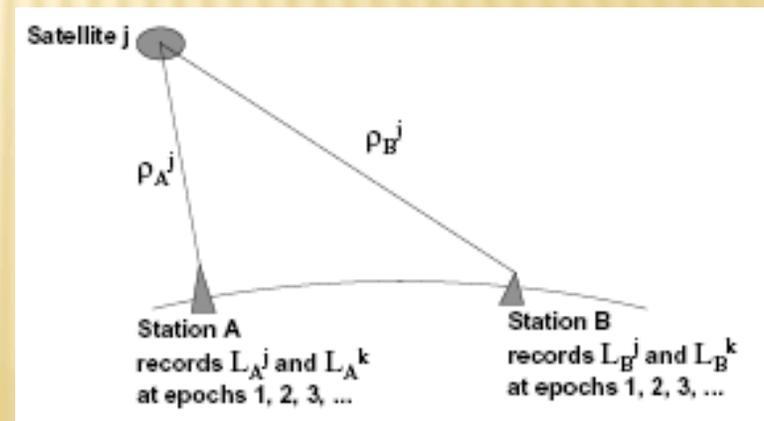
Define the single difference

$$L_A^j(T_A) = \rho_A^j(t_A, t^j) + c\tau_A - c\tau^j + Z_A^j - I_A^j + B_A^j$$

$$L_B^j(T_B) = \rho_B^j(t_B, t^j) + c\tau_B - c\tau^j + Z_B^j - I_B^j + B_B^j$$

$$\Delta L_{AB}^j = L_A^j(T_A) - L_B^j(T_B)$$

Use triangle to remember is
difference between satellite
(top) and two receivers
(bottom)



$$\Delta L_{AB}^j = L_A^j(T_A) - L_B^j(T_B)$$

$$\Delta L_{AB}^j = \rho_A^j - \rho_B^j + c\tau_A - c\tau_B - \cancel{c\tau^j} + \cancel{c\tau^j} \\ + Z_A^j - Z_B^j - I_A^j + I_B^j + B_A^j - B_B^j$$

$$\Delta L_{AB}^j = \Delta\rho_{AB}^j + \Delta c\tau_{AB} + \Delta Z_{AB}^j - \Delta I_{AB}^j + \Delta B_{AB}^j$$

Satellite time errors cancel

(assume transmission times are same – probably not unless range to both receivers from satellite the same)

If the two receivers are close together the tropospheric and ionospheric terms also (approximately) cancel.

How about we do this trick again

This time using two single differences to two satellites

(all at same epoch)

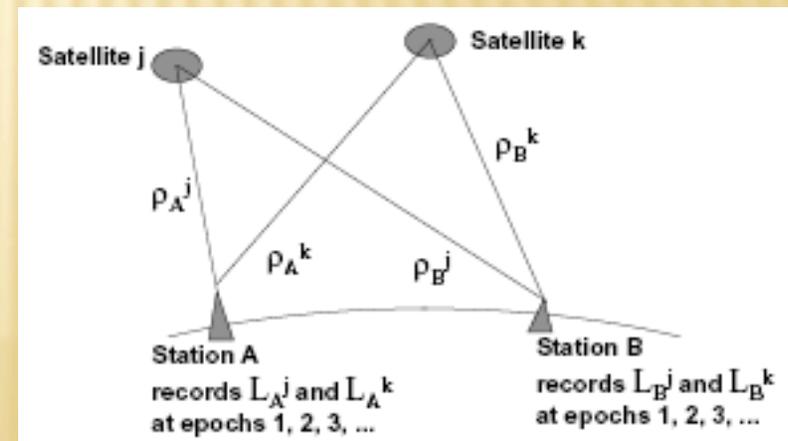
Define the double difference

$$\Delta L_{AB}^j = \Delta \rho_{AB}^j + \Delta c\tau_{AB} + \Delta Z_{AB}^j - \Delta I_{AB}^j + \Delta B_{AB}^j$$

$$\Delta L_{AB}^k = \Delta \rho_{AB}^k + \Delta c\tau_{AB} + \Delta Z_{AB}^k - \Delta I_{AB}^k + \Delta B_{AB}^k$$

$$\nabla \Delta L_{AB}^{jk} = \Delta L_{AB}^j - \Delta L_{AB}^k$$

Use inverted triangle to remember is difference between two satellites (top) and one receiver (bottom)



$$\nabla \Delta L_{AB}^{jk} = \Delta \rho_{AB}^j - \Delta \rho_{AB}^k + \Delta c \tau_{AB} - \Delta c \tau_{AB} \\ + \Delta Z_{AB}^j - \Delta Z_{AB}^k + \Delta I_{AB}^j - \Delta I_{AB}^k + \Delta B_{AB}^j - \Delta B_{AB}^k$$

$$\nabla \Delta L_{AB}^{jk} = \nabla \Delta \rho_{AB}^{jk} + \nabla \Delta Z_{AB}^{jk} - \nabla \Delta I_{AB}^{jk} + \nabla \Delta B_{AB}^{jk}$$

Now we have gotten rid of the receiver clock bias terms (again to first order ~ and results better for short baselines)

Double differencing

- removes (large) clock bias errors
- approximately doubles (smaller) random errors due to atmosphere, ionosphere, etc. (no free lunch)
- have to be able to see satellite from both receivers.

Next – what is the ambiguity term after double difference

(remembering definition of B_A^j)

$$\nabla \Delta B_{AB}^{jk} = \Delta B_{AB}^j - \Delta B_{AB}^k$$

$$\nabla \Delta B_{AB}^{jk} = (B_A^j - B_B^j) - (B_A^k - B_A^k)$$

$$\begin{aligned} \nabla \Delta B_{AB}^{jk} &= \lambda_0 (\phi_{0_A} - \phi_0^j - N_A^j) - \lambda_0 (\phi_{0_B} - \phi_0^j - N_B^j) + \\ &\quad - \lambda_0 (\phi_{0_A} - \phi_0^k - N_A^k) + \lambda_0 (\phi_{0_B} - \phi_0^k - N_B^k) \end{aligned}$$

$$\nabla \Delta B_{AB}^{jk} = -\lambda_0 (N_A^j - N_B^j - N_A^k + N_B^k)$$

$$\nabla \Delta B_{AB}^{jk} = -\lambda_0 N_{AB}^{jk}$$

The ambiguity term reduces to an integer

So our final
Double difference observation
is

$$\nabla\Delta L_{AB}^{jk} = \nabla\Delta\rho_{AB}^{jk} + \nabla\Delta Z_{AB}^{jk} - \nabla\Delta I_{AB}^{jk} - \lambda_0 \nabla\Delta N_{AB}^{jk}$$

One can do the differencing in either order
The sign on the ambiguity term is arbitrary

We seem to be on a roll here, so let's do it again.

This time
(take the difference of double differences)
between two epochs

$$\nabla\Delta L_{AB}^{jk}(i) = \nabla\Delta\rho_{AB}^{jk}(i) + \nabla\Delta Z_{AB}^{jk}(i) - \nabla\Delta I_{AB}^{jk}(i) - \nabla\Delta N_{AB}^{jk}(i)$$

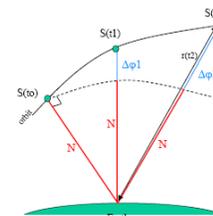
$$\nabla\Delta L_{AB}^{jk}(i+1) = \nabla\Delta\rho_{AB}^{jk}(i+1) + \nabla\Delta Z_{AB}^{jk}(i+1) - \nabla\Delta I_{AB}^{jk}(i+1) - \nabla\Delta N_{AB}^{jk}(i+1)$$

$$\delta(i, i+1)\nabla\Delta L_{AB}^{jk} = \nabla\Delta L_{AB}^{jk}(i+1) - \nabla\Delta L_{AB}^{jk}(i)$$

Equal if no
loss of lock
(no cycle
slip)

Phase measurements

- When a satellite is locked (at t_0), the GPS receiver starts tracking the incoming phase
- It counts the (real) number of phases as a function of time = $\Delta\phi(t)$
- But the initial number of phases N at t_0 is unknown...
- However, if no loss of lock, N is constant over an orbit arc



From E. Calais

So now we have gotten rid of the integer ambiguity

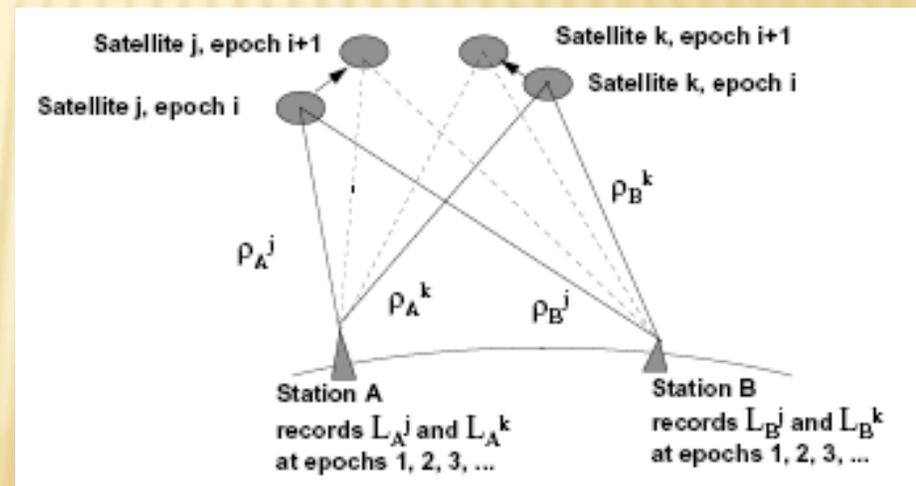
$$\delta(i, i+1) \Delta L_{AB}^{jk} = \nabla \Delta L_{AB}^{jk}(i+1) - \nabla \Delta L_{AB}^{jk}(i)$$

$$\delta(i, i+1) \Delta L_{AB}^{jk} = \delta(i, i+1) \nabla \Delta \rho_{AB}^{jk}(i) +$$

$$\delta(i, i+1) \nabla \Delta Z_{AB}^{jk}(i) - \delta(i, i+1) \nabla \Delta I_{AB}^{jk}(i)$$

If no cycle slip –
ambiguities removed.

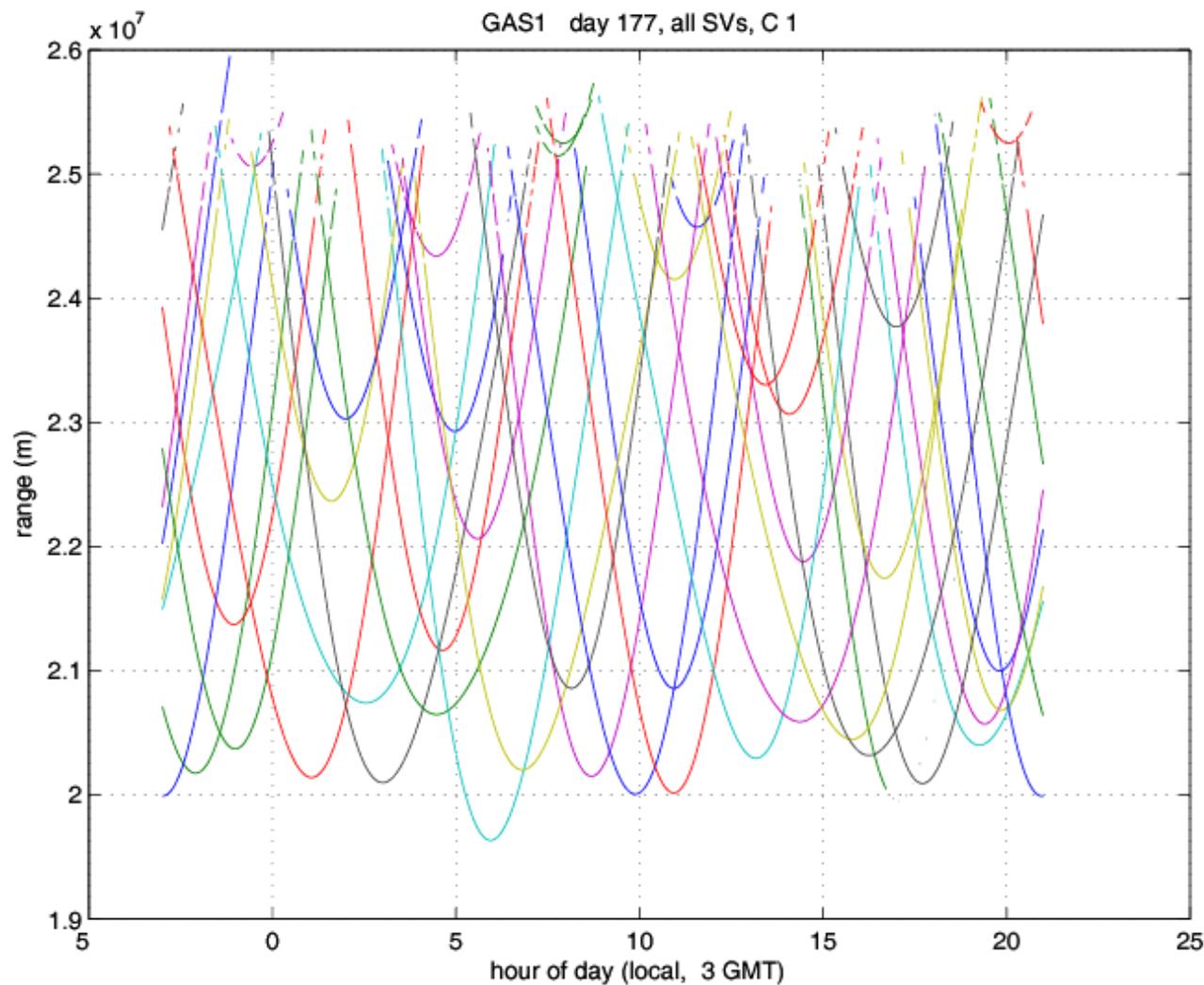
If there is a cycle slip – get
a spike in the triple
difference.



Raw Data from RINEX file: RANGE

Plot of C1 (range in meters)

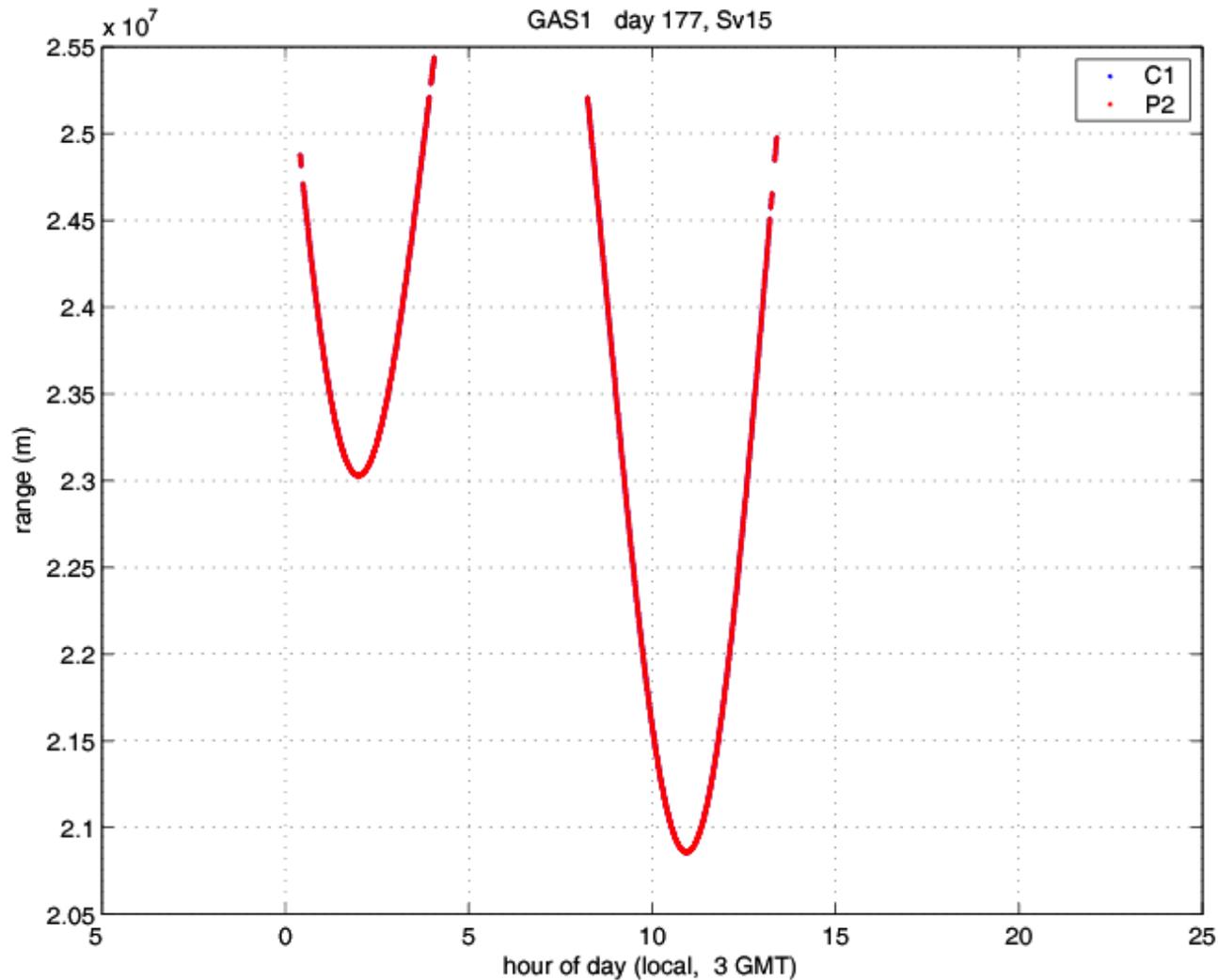
For all satellites for full day of data



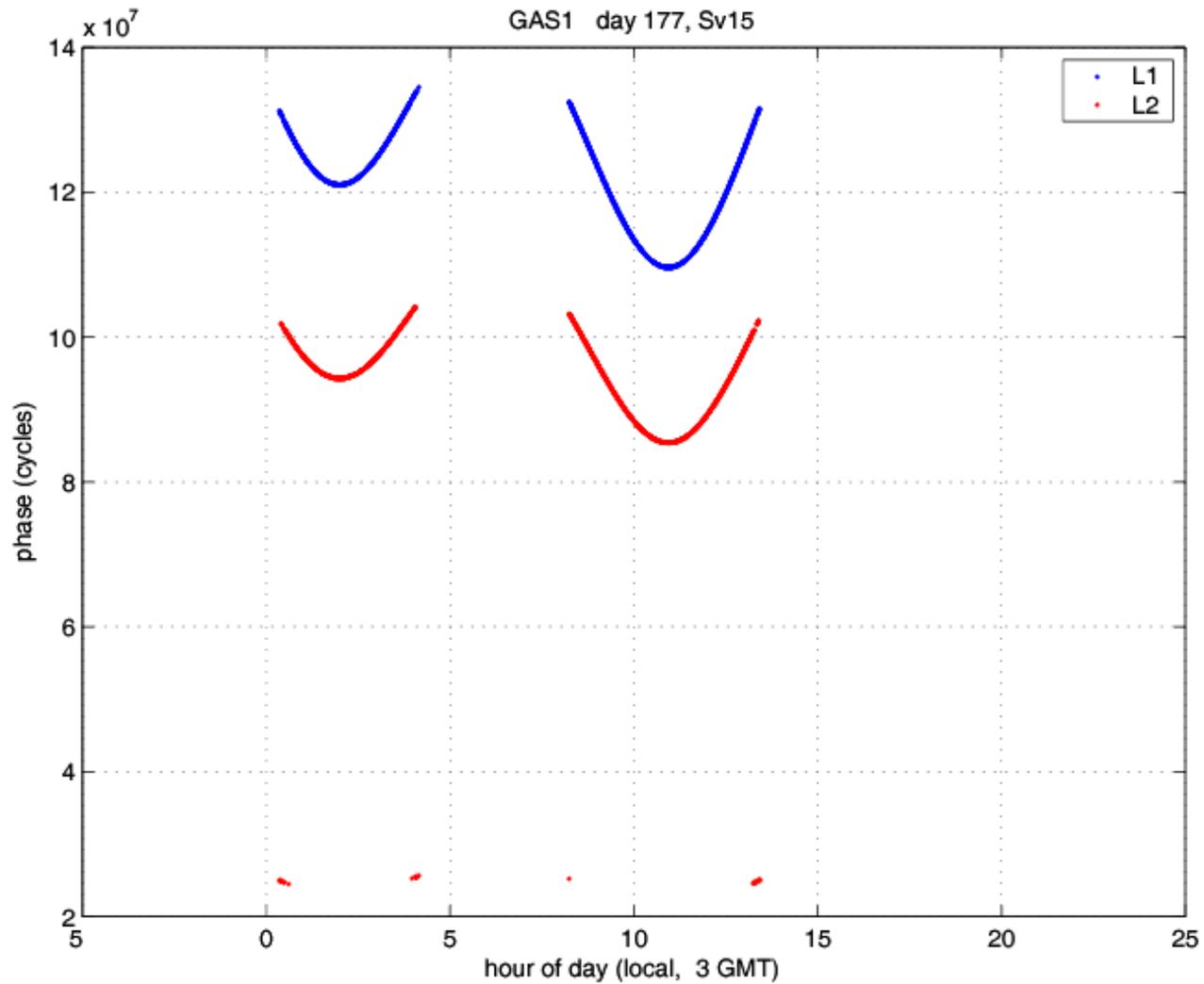
Raw Data from RINEX file: RANGE

Plot of P1 (range in meters)

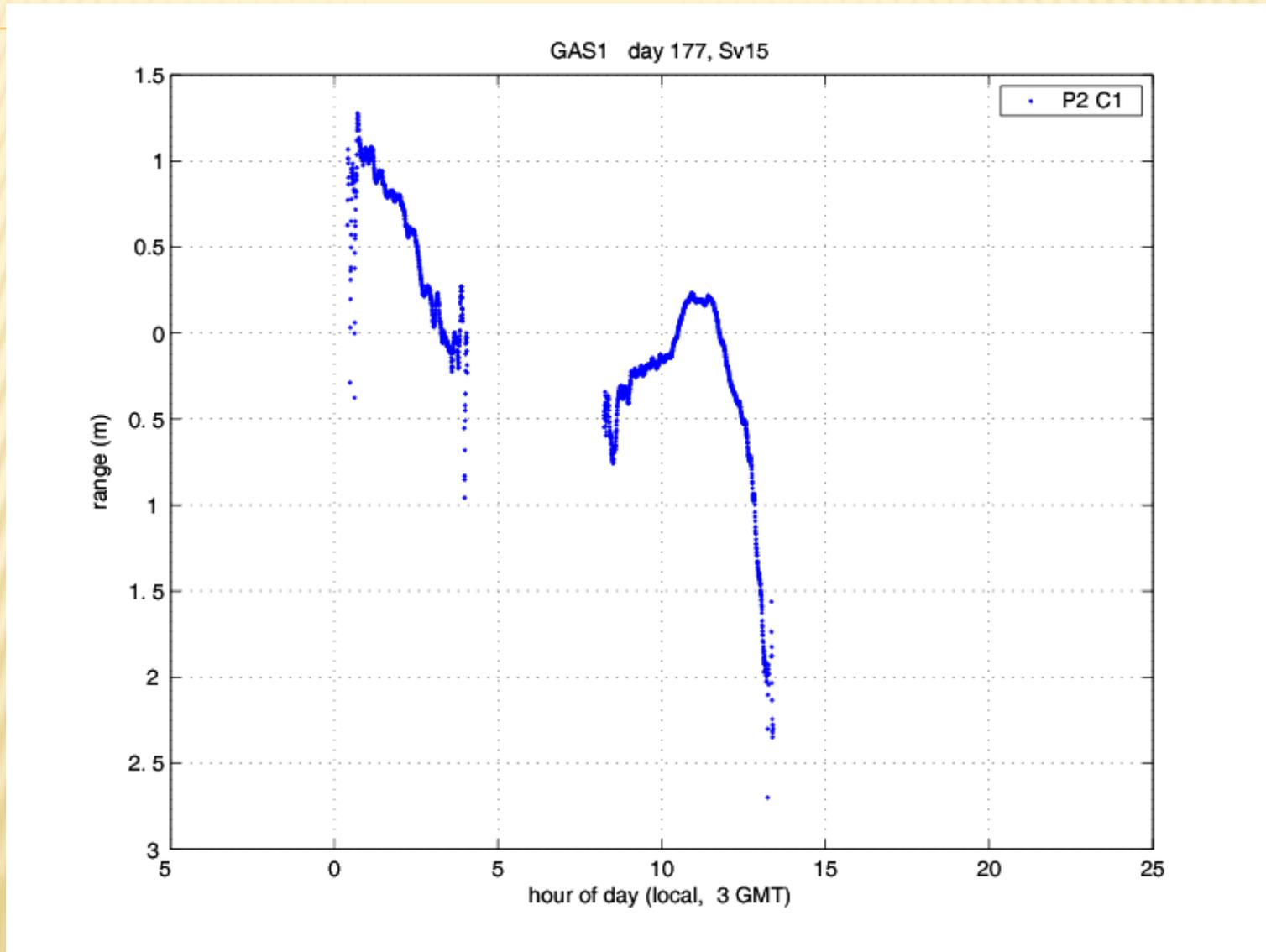
For one satellite for full day of data



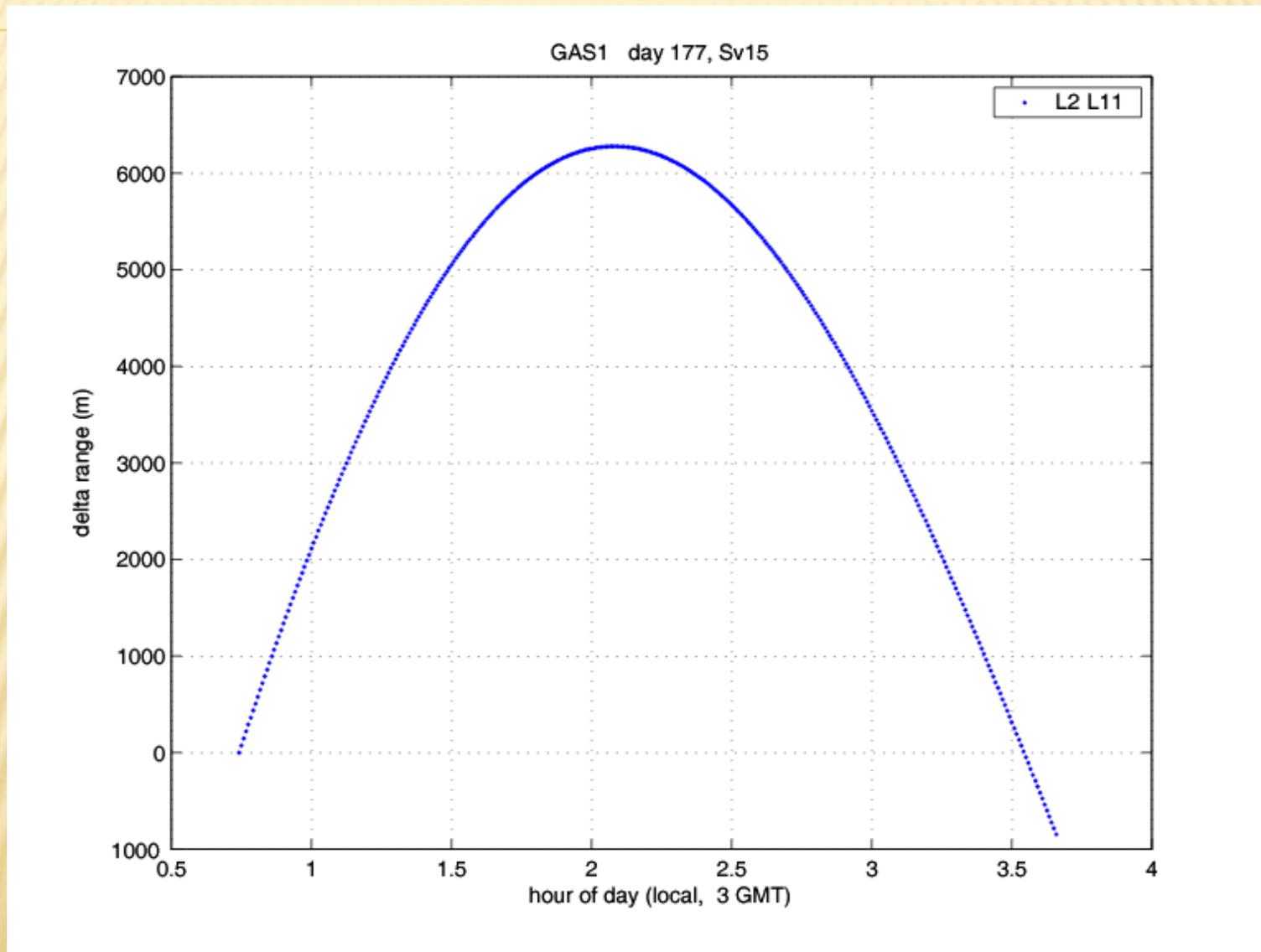
Raw Data from RINEX file: PHASE



Raw Data from RINEX file: RANGE DIFFERENCE

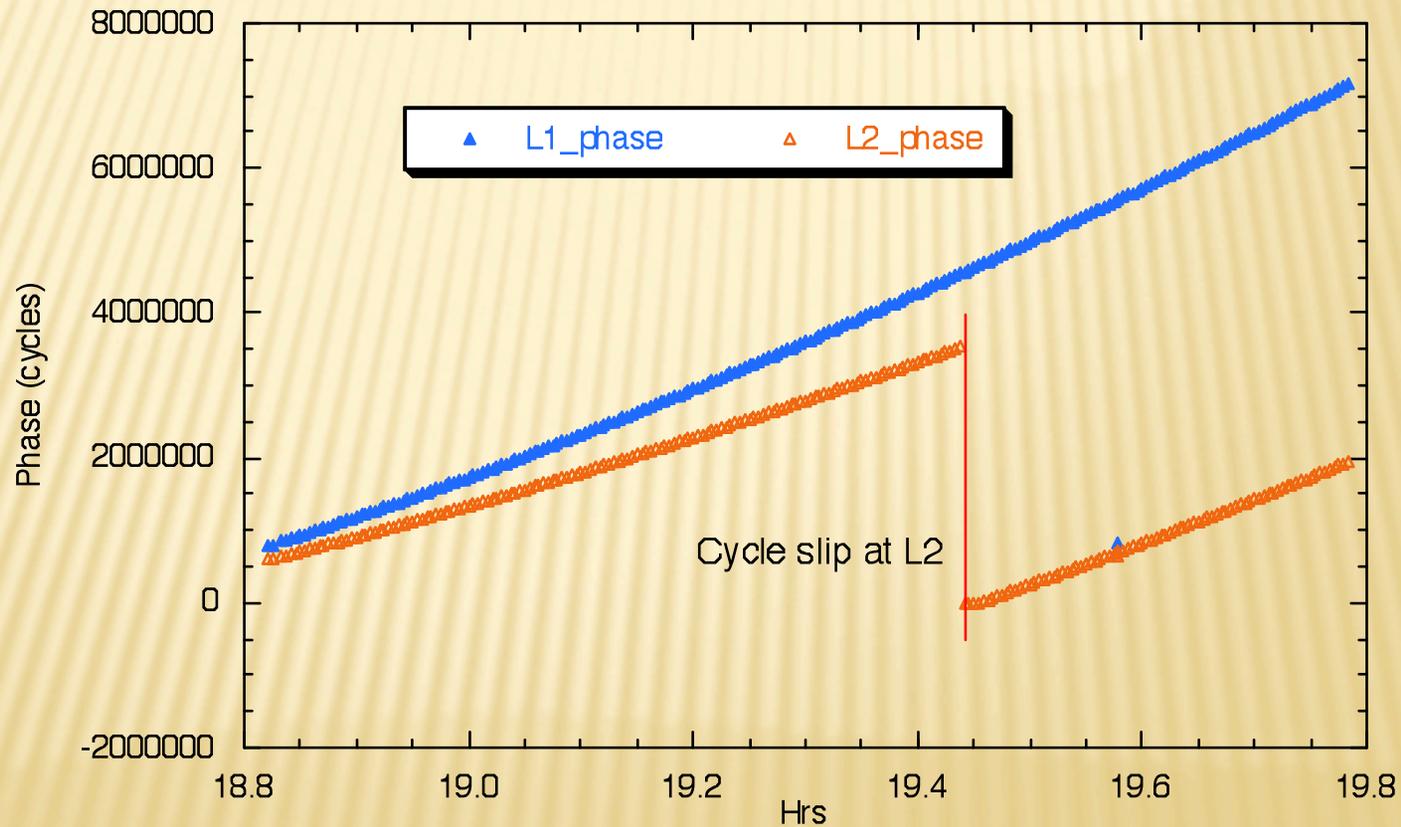


Raw Data from RINEX file: PHASE DIFFERENCE

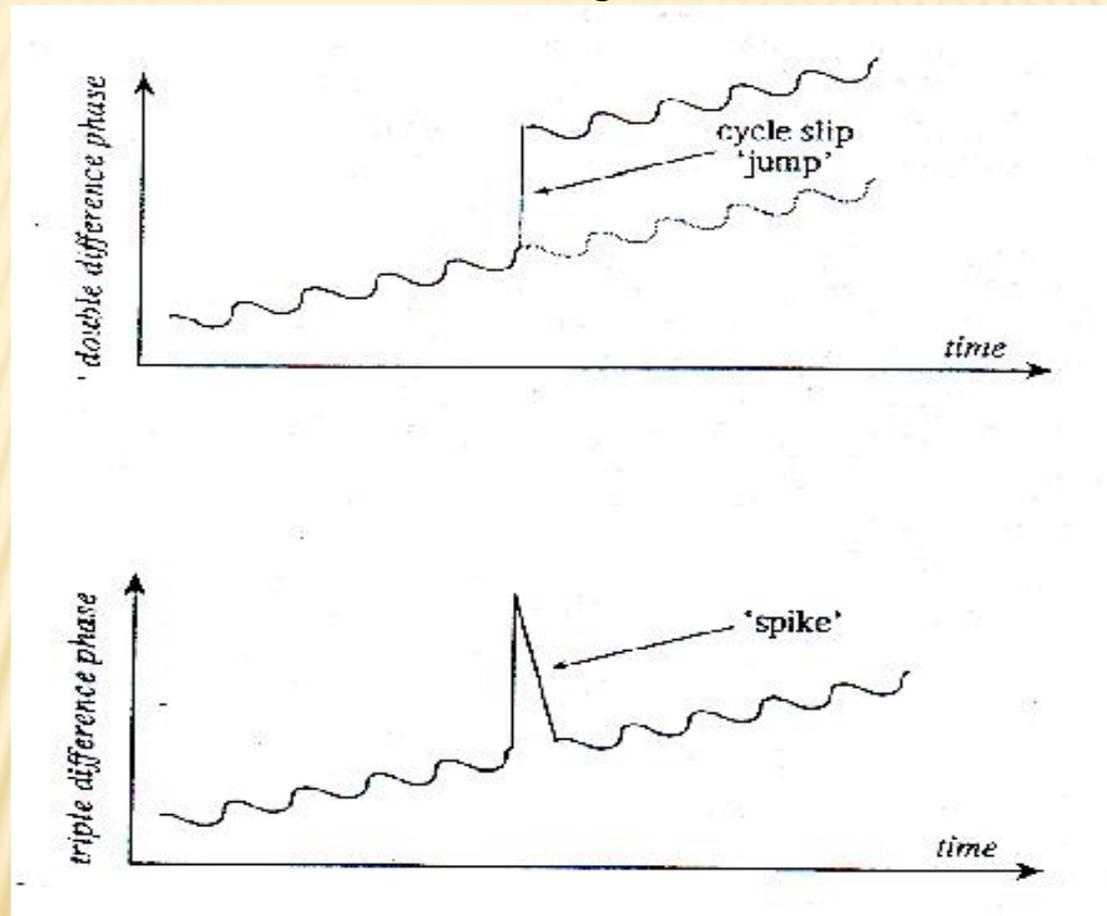


Zoom in on phase observable

Without an (L1) and with an (L2) cycle slip



Cycle slip shows up as spike in triple difference
(so can identify and fix)



Have to do this for “all” pairs of receiver-satellite pairs.

Effects of triple differences on estimation

Further increase in noise
Additional effect – introduces
correlation between observations in time

This effect substantial

So triple differences limited to identifying and fixing
cycle slips.

Using double difference phase observations for relative positioning

First notice that if we make all double differences - even ignoring the obvious duplications

$$\nabla \Delta L_{AB}^{jk} = \nabla \Delta L_{AB}^{kj} = \nabla \Delta L_{BA}^{kj} = \nabla \Delta L_{BA}^{jk}$$

We get a lot more double differences than original data.

This can't be (can't create information).

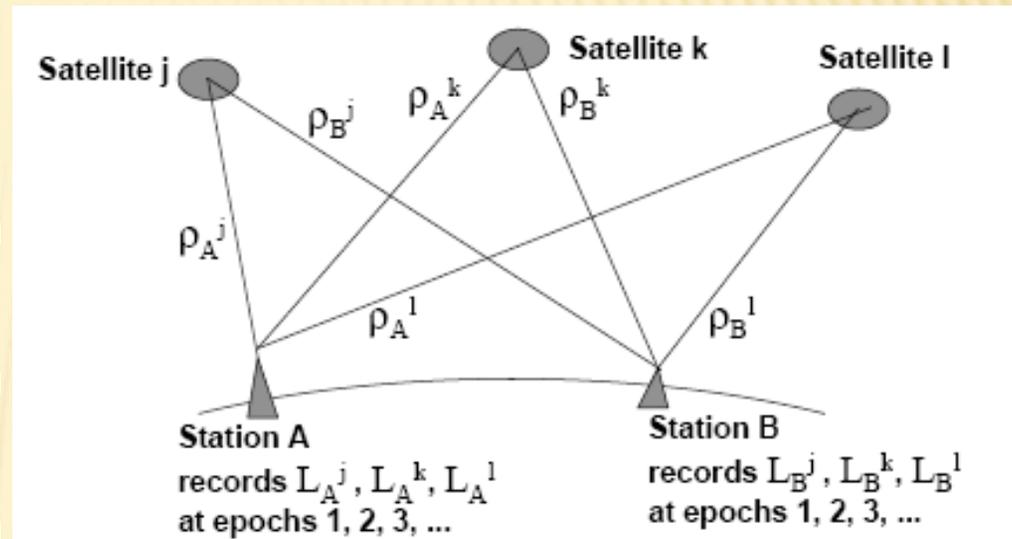
Consider the case of 3 satellites observed by 2 receivers.

Form the (non trivial)
double differences

$$L_{AB}^{jk} = (L_A^j - L_B^j) - (L_A^k - L_B^k)$$

$$L_{AB}^{jl} = (L_A^j - L_B^j) - (L_A^l - L_B^l)$$

$$L_{AB}^{lk} = (L_A^l - L_B^l) - (L_A^k - L_B^k)$$



Note that we can form any one
from a linear combination of the
other two

(linearly dependent)

We need a linearly independent set for Least Squares.

$$L_{AB}^{jk} = L_{AB}^{jl} - L_{AB}^{lk}$$

$$L_{AB}^{jl} = L_{AB}^{jk} - L_{AB}^{lk}$$

$$L_{AB}^{lk} = L_{AB}^{jk} - L_{AB}^{jl}$$

From the linearly dependent set

$$\left\{ L_{AB}^{jk}, L_{AB}^{jl}, L_{AB}^{lk} \right\}$$

We can form a number of linearly independent subsets

$$\left\{ L_{AB}^{jk}, L_{AB}^{jl} \right\} = \Lambda^j = \left\{ L_{AB}^{ab} \mid a = j; b \neq j \right\}$$

$$\left\{ L_{AB}^{kj}, L_{AB}^{kl} \right\} = \Lambda^k = \left\{ L_{AB}^{ab} \mid a = k; b \neq k \right\}$$

$$\left\{ L_{AB}^{lj}, L_{AB}^{lk} \right\} = \Lambda^l = \left\{ L_{AB}^{ab} \mid a = l; b \neq l \right\}$$

Which we can then use for our Least Squares estimation.

How to pick the basis?

All linearly independent sets are “equally” valid
and should produce identical solutions.

Pick Λ' such that reference satellite / has data at every
epoch

Better approach is to select the reference satellite
epoch by epoch

(if you have 24 hour data file, cannot pick one satellite
and use all day ~ no satellite is visible all day)

For a single baseline (2 receivers) that observe s satellites,
the number of linearly independent double difference observations is

$$s-1$$

Next suppose we have more than 2 receivers.

We have the same situation

-all the double differences are not linearly independent.

As we just did for multiple satellites, we can pick a
reference station

that is common to all the double differences.

For a network of r receivers,
the number of linearly independent double difference
observations is

$$r-1$$

So all together we have a total of

$$(s-1)(r-1)$$

Linearly independent double differences

So our linearly independent set of double differences is

$$\Lambda_C^j = \left\{ L_{AB}^{ab} \mid a = j; b \neq j; A = C, B \neq C \right\}$$

Reference station method has problems when all receivers can't see all satellites at the same time.

Choose receiver close to center of network.

Even this might not work when the stations are very far apart.

For large networks may have to pick short baselines that connect the entire network.

Idea is to not have any closed polygons (which give multiple paths and therefore be linearly dependent) in the network.

Can also pick reference station epoch per epoch.

If all the receivers see the same satellites at each epoch,
and data weighting is done properly,
then it does not matter which receiver and satellite we
pick for the reference.

In practice, however,
the solution depends on our choices of reference
receiver and satellite.

(although the solutions should be similar)

(could process all undifferenced phase observations
and estimate clocks at each epoch – ideally gives
“better” estimates)

Double difference observation equations

Start with

$$\nabla\Delta L_{AB}^{jk} = \nabla\Delta\rho_{AB}^{jk} + \nabla\Delta Z_{AB}^{jk} - \nabla\Delta I_{AB}^{jk} - \nabla\Delta N_{AB}^{jk}$$

Simplify to

$$L_{AB}^{jk} = \rho_{AB}^{jk} - \lambda_0 N_{AB}^{jk}$$

By dropping the $\nabla\Delta$

And assuming $\nabla\Delta Z_{AB}^{jk}$ & $\nabla\Delta I_{AB}^{jk}$ are negligible

Processing double differences between two receivers
results in a

Baseline solution

The estimated parameters include the vector between
the two receivers (actually antenna phase centers).

May also include estimates of parameters to model
troposphere (statistical) and ionosphere (measured –
dispersion).

Also have to estimate the

Integer Ambiguities

For each set of satellite-receiver double differences

We are faced with the same task we had before when we
used

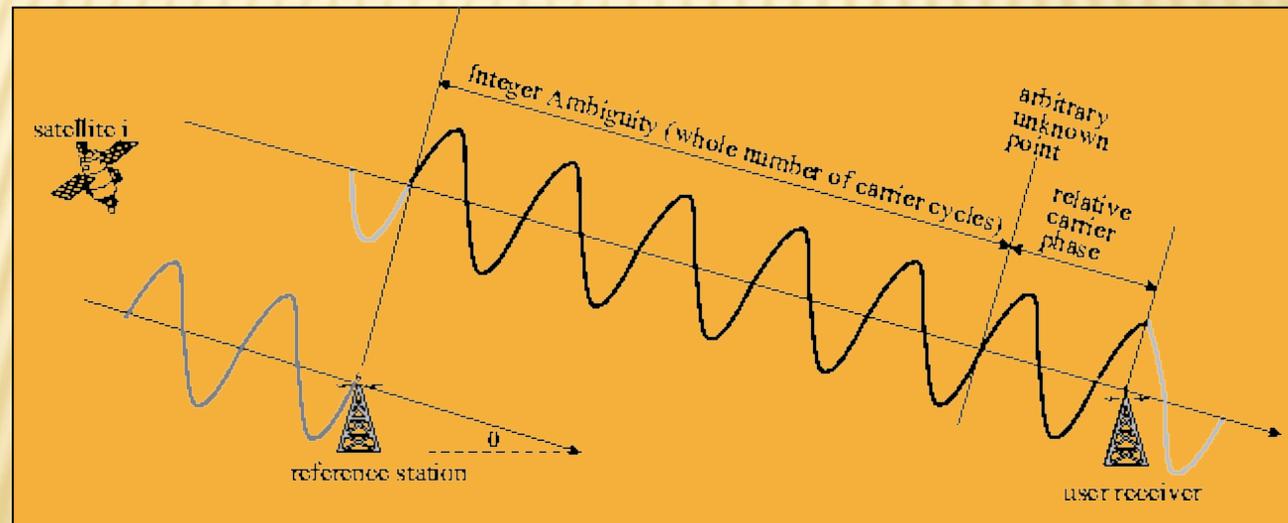
pseudo range

We have to

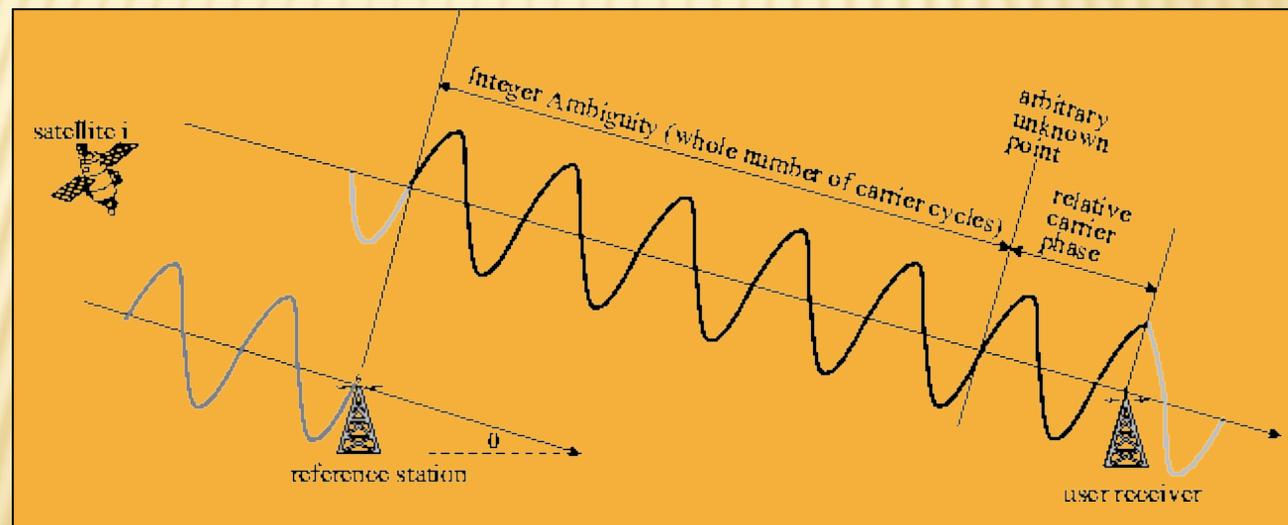
linearize

the problem in terms of the parameters we want to
estimate

A significant difference between using the pseudo range, which is a stand alone method, and using the Phase, is that the phase is a differential method (similar to VLBI).

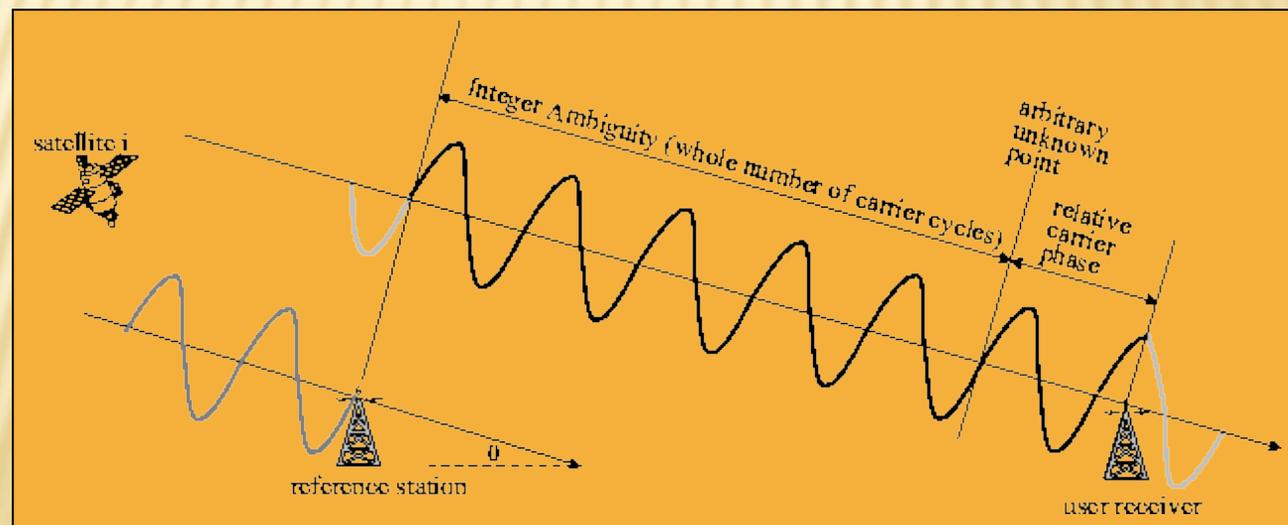


So far we have cast the problem in terms of the distances
to
the satellites,
but we could recast it in terms of the relative distances
between stations.



So now we will need multiple receivers.
We will also have to use (at least one) as a reference station.

In addition to knowing where the satellites are,
We need to know the position of the reference station(s)
to the same level of precision as we wish to estimate the
position of the other stations.



fiducial positioning

Fiducial

Regarded or employed as a standard of reference, as in surveying.

So now we have to assign the location of our fiducial station(s)

Can do this with

RINEX header position

VLBI position

Other GPS processing

etc.

So we have to

Write down the equations

Linearize

Solve