

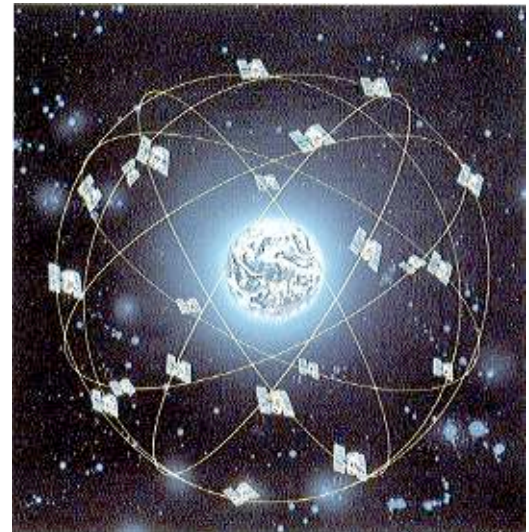
Satellite Orbits

Keplerian motion
Perturbed motion
GPS satellites
GPS orbits

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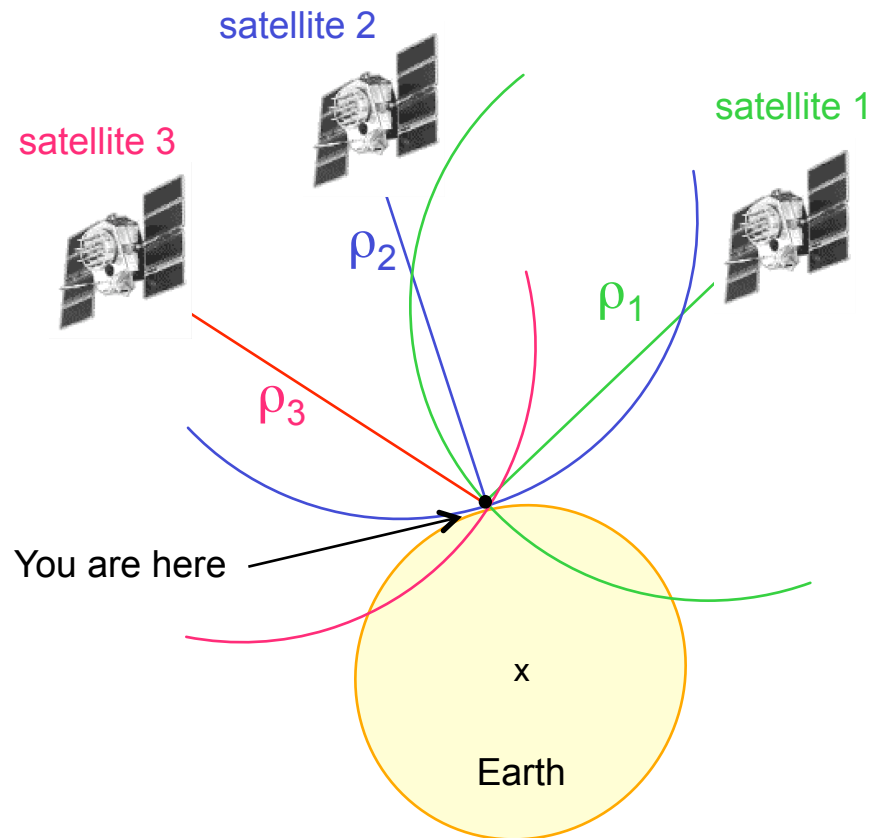


Orbits?



© 1980 Sidney Harris. This cartoon was originally published in American Scientist.

Satellite orbits: What for?



- Principle of GPS positioning:
 - Satellite 1 sends a signal at time t_{e1}
 - Ground receiver receives it signal at time t_r
 - The range measurement ρ_1 to satellite 1 is:
 - $\rho_1 = (t_r - t_{e1}) \times \text{speed of light}$
 - We are therefore located on a sphere centered on satellite 1, with radius ρ_1
 - 3 satellites => intersection of 3 spheres
- The mathematical model is:
$$\rho_r^s = \sqrt{(X_s - X_r)^2 + (Y_s - Y_r)^2 + (Z_s - Z_r)^2}$$
 - GPS receivers measure ρ_r^s
 - If the position of the satellites in an Earth-fixed frame (X_s, Y_s, Z_s) is known,
 - Then one can solve for (X_r, Y_r, Z_r) (if at least 3 simultaneous range measurements)

Dynamics of satellite orbits

- Basic dynamics in an inertial frame described by: $\sum \vec{F} = m\vec{a}$
- Case of two-body problem (two point masses), forces are:
 - Gravitational forces
 - Solar radiation pressure (drag is negligible for GPS)
 - Thruster firings (not directly modeled).
- Neglecting radiation pressure, one can write:

$$\vec{F} = \frac{Gm_s m_E}{r^2} \vec{r} \quad \text{and} \quad \vec{F} = m_s \vec{a}$$
$$\Rightarrow \vec{a} - \frac{Gm_E}{r^2} \vec{r} = \vec{0} \Leftrightarrow \boxed{\frac{d^2 \vec{r}}{dt^2} = \frac{Gm_E}{r^2} \vec{r}}$$

- r = geocentric position vector
- $a = d^2r/dt^2$, relative acceleration vector
- G = universal gravitational constant
- m_E = Earth's mass
- m_s = satellite's mass

$$m_s \ddot{\vec{r}}_s = -G \frac{m_s m_E}{r^2} \vec{r}$$

$$m_E \ddot{\vec{r}}_E = G \frac{m_s m_E}{r^2} \vec{r}$$

$$r = \|\vec{r}_s - \vec{r}_E\|$$

$$\vec{r} = \frac{\vec{r}_s - \vec{r}_E}{r}$$

$$\ddot{\vec{r}}_s - \ddot{\vec{r}}_E = -G \frac{m_E}{r^2} \vec{r} - G \frac{m_s}{r^2} \vec{r}$$

$$\Rightarrow \ddot{\vec{r}} = -G(m_s + m_E) \frac{\vec{r}}{r^2}$$

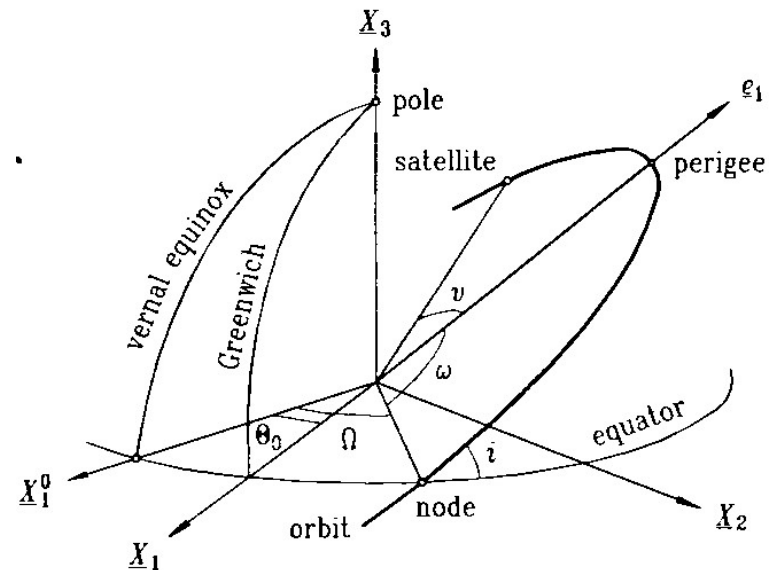
$$\ddot{\vec{r}} = -\mu \frac{\vec{r}}{r^2}$$

$$\mu = G(m_s + m_E)$$

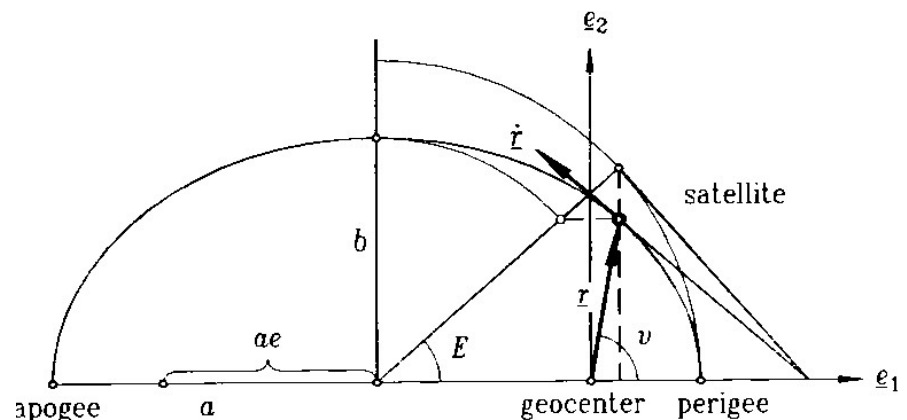
Keplerian motion

Analytical solution to this force model = Keplerian (= osculating) orbit:

- Six integration constants => 6 orbital parameters or Keplerian (= osculating) elements
- In an **inertial** reference frame, orbits can be described by an ellipse
- The orbit plane stays fixed in space
- One of the foci of the ellipse is the center of mass of the body
- These orbits are described by Keplerian elements:



a	Semi-major axis	Size and shape of orbit
e	Eccentricity	
Ω	Right ascension of ascending node	Orientation of the orbital plane in the inertial system
ω	Argument of perigee	
i	Inclination	
T_0	Epoch of perigee	Position of the satellite in the orbital plane



Keplerian motion

- Third Kepler's law (period²/*a*³=const.) relate mean angular velocity *n* and revolution period *P*:

$$n = \frac{2\pi}{P} = \sqrt{\frac{GM_E}{a^3}}$$

- M_E = Earth's mass, $GM_E = 3,986,005 \times 10^8 \text{ m}^3\text{s}^{-2}$
- For GPS satellites:
 - Nominal semi-major axis $a = 26\,560,000 \text{ m}$
 - Orbital period = 12 sidereal hours (= 11h28mn UT), $v=3.87 \text{ km/s}$
 - Therefore, positions of GPS satellites w.r.t. Earth's surface repeat every sidereal day

Keplerian motion

- Instantaneous position of a satellite on its orbit is defined by angular quantities called “*anomalies*”:

- Mean anomaly: $M(t) = n \times (t - T_0)$

with n = mean motion = number of orbits in 24 hours, T_0 = time of perigee

- Eccentric anomaly: $E(t) = M(t) + e \sin E(t)$

- True anomaly: $v(t) = 2 \operatorname{atan} \left[\frac{(1+e)}{(1-e)} \right]^{1/2} \tan(E(t)/2)$

- In the coordinate system defined by the **orbital plane**:

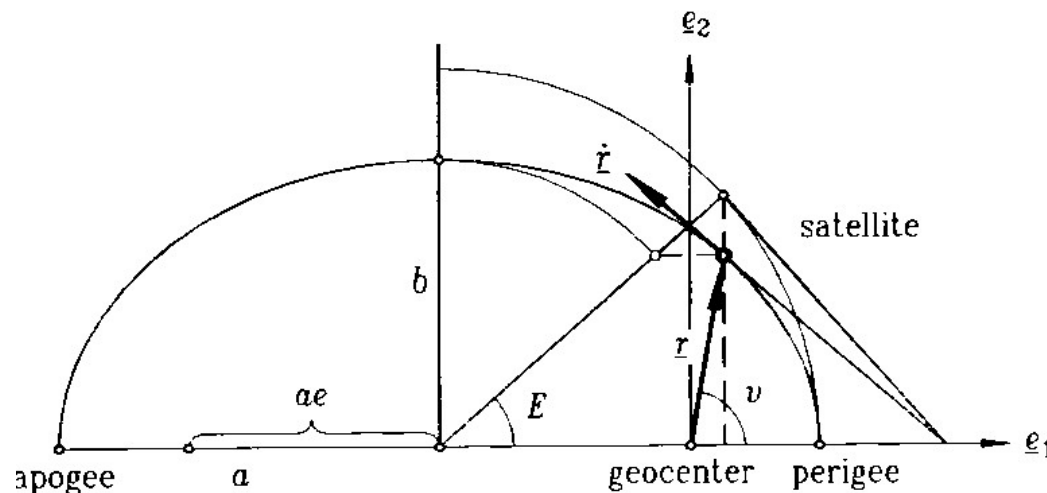
- $e_1 = r \cos v = a \cos E - ae = a (\cos E - e)$

- $e_2 = r \sin v = (b/a) a \sin E = b \sin E = a (1-e^2)^{1/2} \sin E$

- $e_3 = 0$

$$\vec{r} = \begin{bmatrix} e_1 \\ e_2 \\ e_3 \end{bmatrix} = \begin{bmatrix} a(\cos E - e) \\ a\sqrt{1-e^2} \sin E \\ 0 \end{bmatrix}$$

$$\|\vec{r}\| = a(1 - e \cos E)$$



Keplerian motion

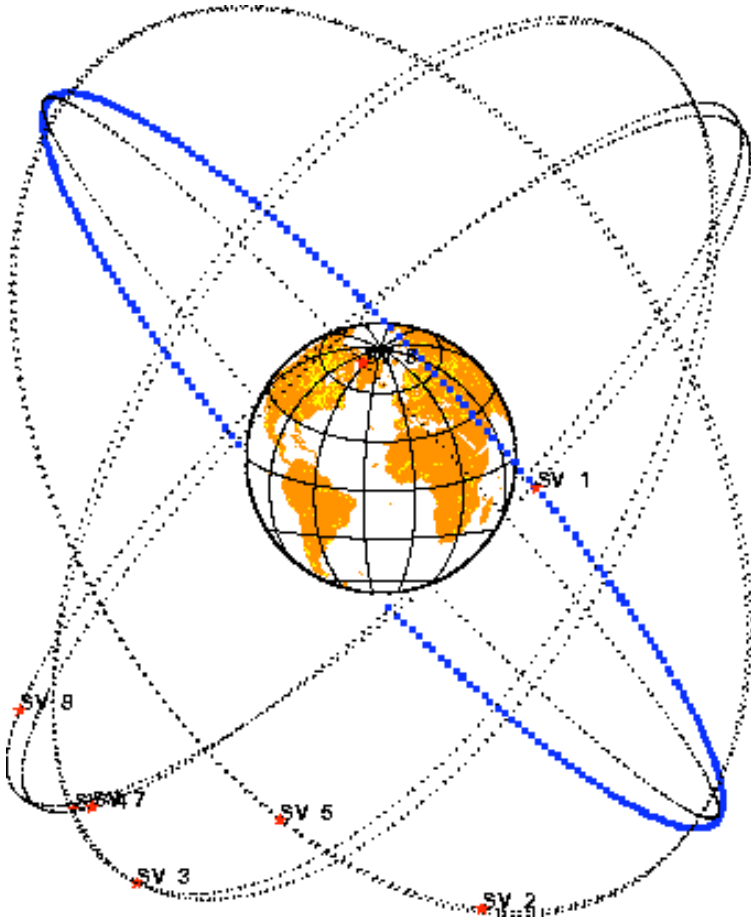


Fig. T. Herring (MIT)

GPS orbit, inertial frame

- GPS orbit in an inertial frame (+Earth rotation)
- To compute site position on the Earth, we need the satellite orbit to an Earth-fixed frame...

Keplerian motion

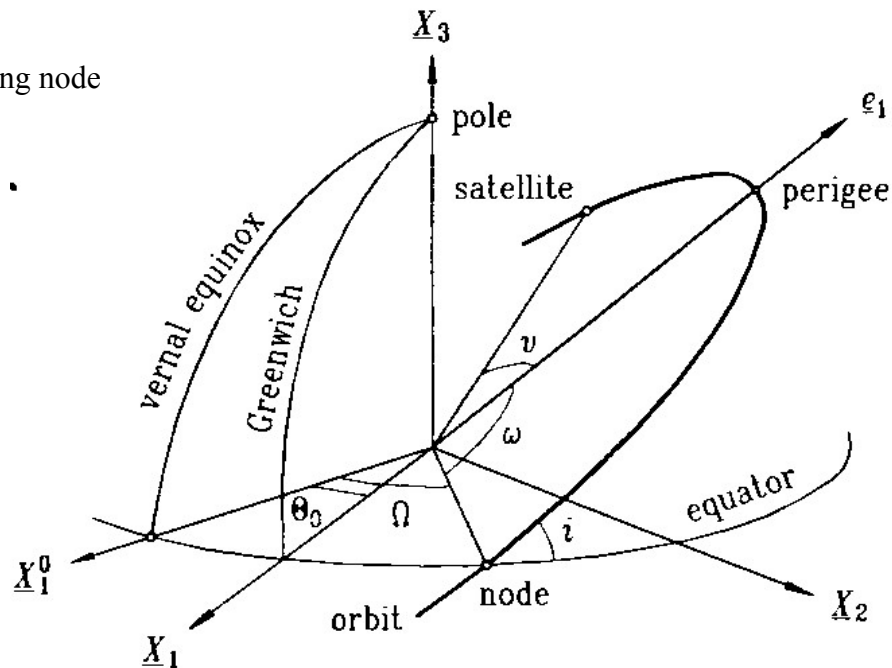
In the Earth centered inertial system ($X_1^0, X_2^0=X_2, X_3^0=X_3$), ρ relates to r through the combination of 3 rotations:

$$\vec{\rho} = R\vec{r}$$

$$R = R_3\{-\Omega\}R_1\{-i\}R_3\{-\omega\} \quad R = \begin{bmatrix} \cos \Omega \cos \omega - \sin \Omega \sin \omega \cos i & -\cos \Omega \sin \omega - \sin \Omega \cos \omega \cos i & \sin \Omega \sin i \\ \sin \Omega \cos \omega + \cos \Omega \sin \omega \cos i & -\sin \Omega \sin \omega + \cos \Omega \cos \omega \cos i & -\cos \Omega \sin i \\ \sin \omega \sin i & \cos \omega \cos i & \cos i \end{bmatrix}$$

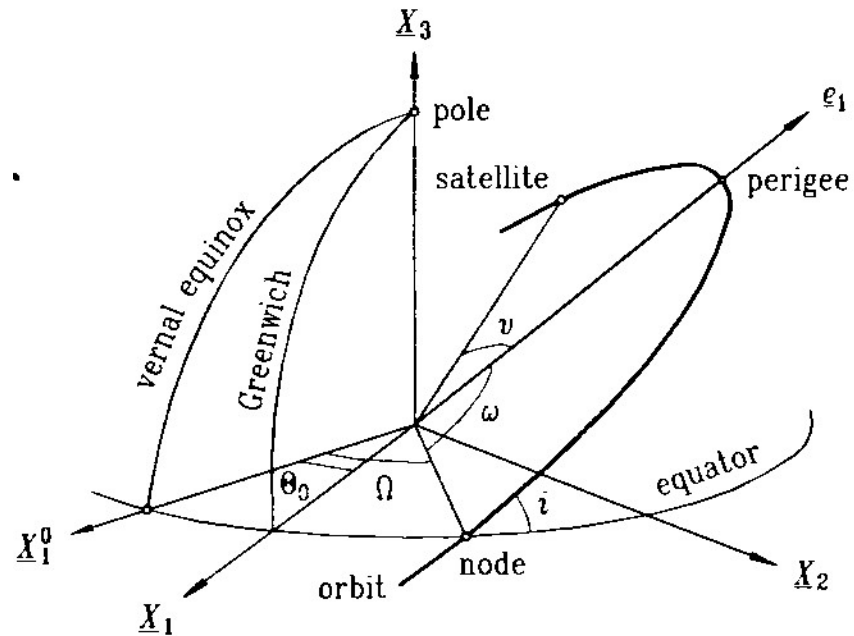
[think of what it takes for (e_1, e_2, e_3) to align with (X_1^0, X_2, X_3)]

Ω = ascension of ascending node
 ω = argument of perigee
 i = inclination
 v = true anomaly



Keplerian motion

- With 3 rotations (Ω, i, ω) , we went from orbital plane coordinates (e_1, e_3, e_3) to Earth-centered inertial coordinates (r)
- To convert r to an **Earth fixed system** (X_1, X_2, X_3) , we need an additional rotation of Θ_o (related to the Greenwich Sidereal Time) about X_3 :



$$\vec{\rho} = R' \vec{r}$$

$$R' = R_3\{\Theta_o\}R = R_3\{\Theta_o\}R_3\{-\Omega\}R_1\{-i\}R_3\{-\omega\}$$

defining: $l = \Omega - \Theta_o$

$$R' = \begin{bmatrix} \cos l \cos \omega - \sin l \sin \omega \cos i & -\cos l \sin \omega - \sin l \cos \omega \cos i & \sin l \sin i \\ \sin l \cos \omega + \cos l \sin \omega \cos i & -\sin l \sin \omega + \cos l \cos \omega \cos i & -\cos l \sin i \\ \sin \omega \sin i & \cos \omega \cos i & \cos i \end{bmatrix}$$

GPS Orbits

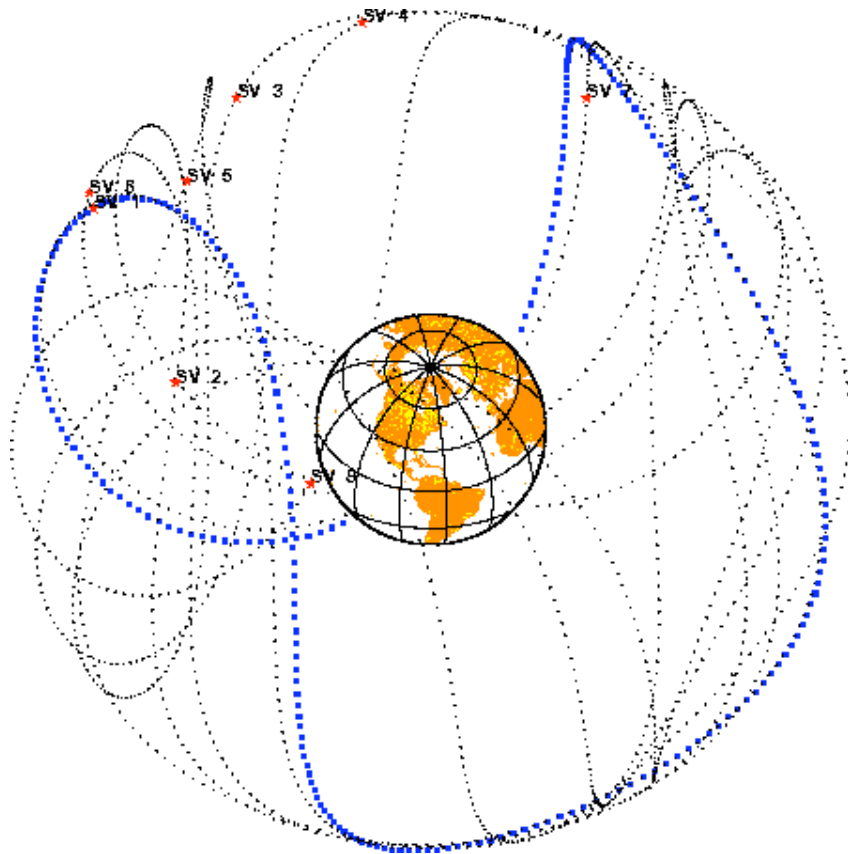


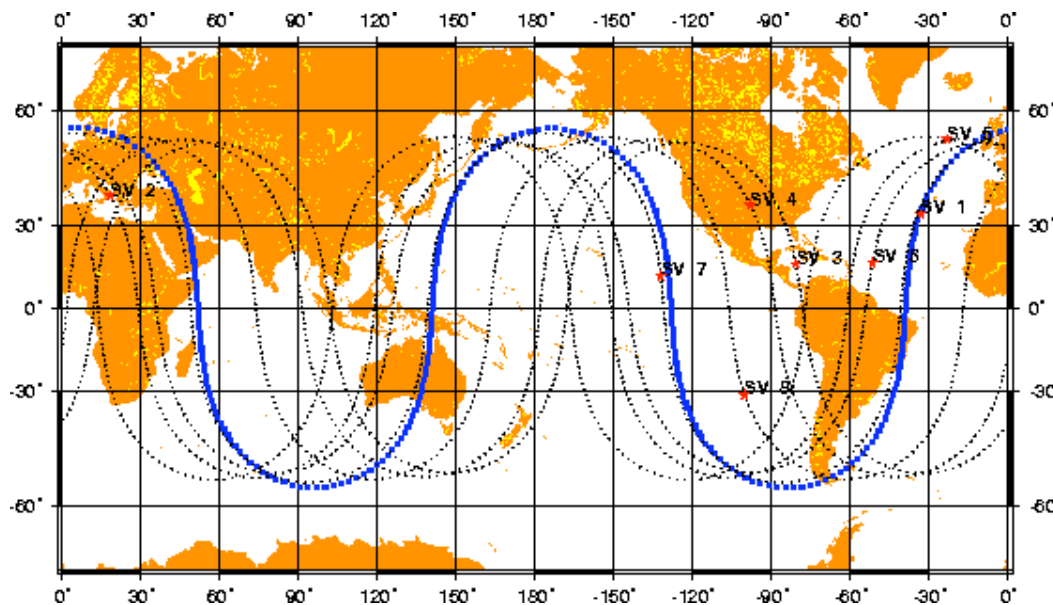
Fig. T. Herring (MIT)

GPS orbit, Earth-fixed frame

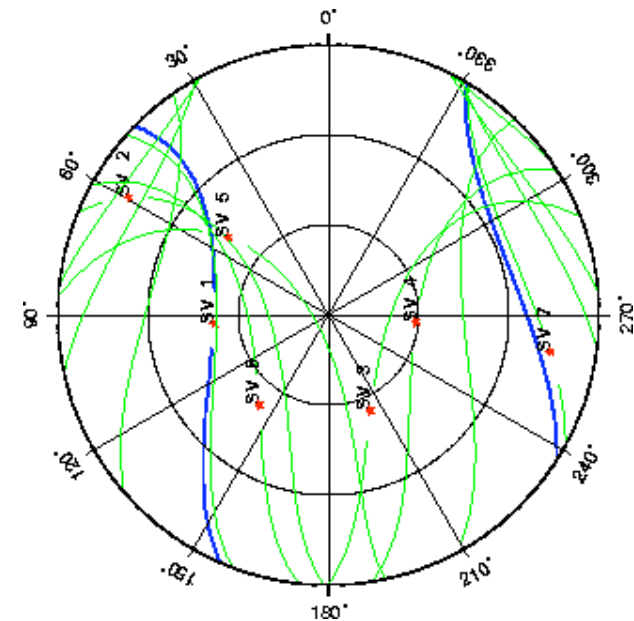
1. Broadcast ephemerides (in GPS signal) contain **orbital parameters** $M, e, a, \Omega, i, \omega, n$ (=angular velocity)
2. Orbital parameters are used to compute orbit in **inertial frame**
3. Orbit in inertial frame is then **rotated into terrestrial frame** (Earth-fixed)
4. In order to do this accurately over long time periods, one need to account for variations in Earth orientation and rotation parameters => use precise UT1, nutations, and polar motion.
5. And take into account orbit perturbations (Earth's gravity field, solar pressure, attraction from Sun and Moon): also provided in broadcast ephemerides

GPS Orbits

Other representations of GPS orbits



GPS orbit in Earth-fixed frame =
“ground track”



GPS orbit in
topocentric frame =
“sky plot”

Perturbed motion

Central gravitational force = main force acting on GPS satellites, but there are other significant perturbations:

- Gravitational forces:
 - Non sphericity of the Earth gravitational potential:
 - Major contribution from the Earth's flattening (J_2)
 - GPS orbits high (20 000 km) and attraction force attenuates rapidly with altitude => only a few terms of the Earth's gravitational potential are necessary for modeling GPS orbits
 - Third body effect: direct attraction of Moon and Sun => lunar and solar ephemerides necessary to model GPS orbits
 - [Tidal effects of Sun and Moon => deforms Earth => modifies Earth's gravitational potential: negligible for GPS satellites]
- Non-gravitational forces:
 - Solar radiation pressure:
 - Impact on the satellite surfaces of photons emitted by the Sun and reflected by the Earth surface: can be modeled, knowing the 3D geometry and the attitude of the satellite.
 - Effects on GPS satellite position: 5-10 m
 - Eclipse periods = satellite in the Earth's shadow (1-2/year, lasts about 1 hr): transition to Sun light difficult to model, usually this part of the orbit is simply edited out!
 - [Atmospheric drag = negligible for GPS satellites]
 - Satellite maneuvers

Solar radiation pressure

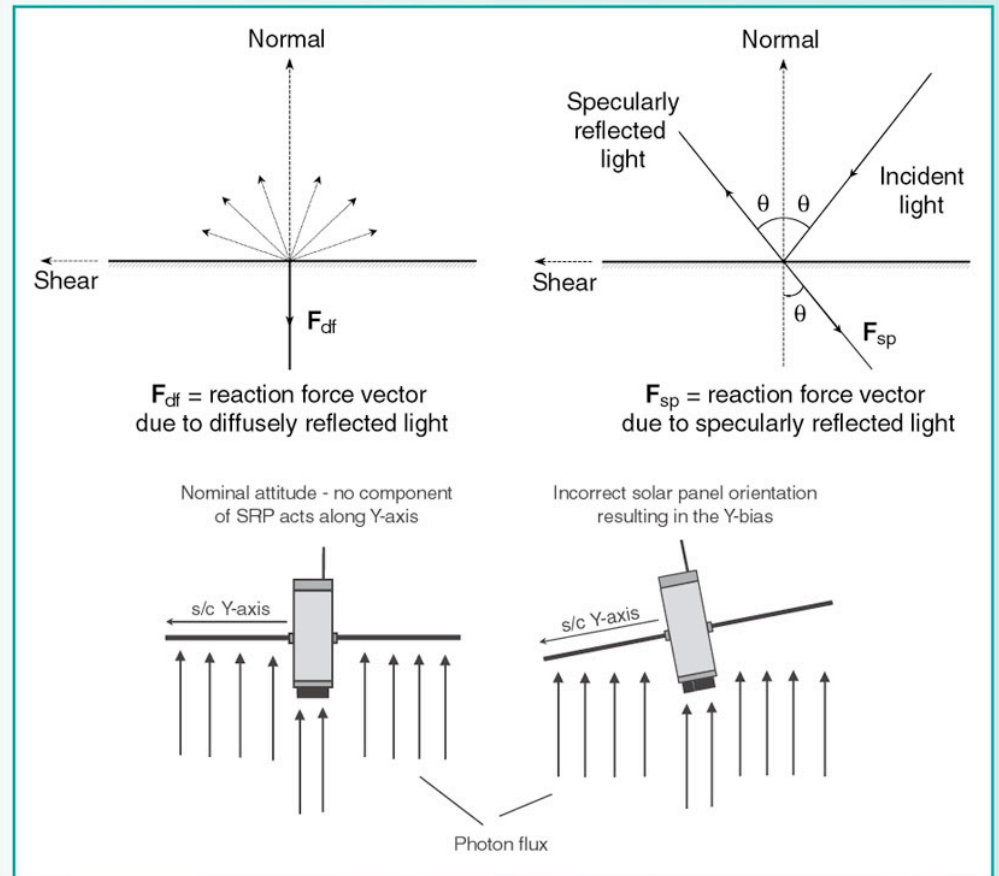
- Results from impact of Sun photons on the satellite's surface.
- Depends on:
 - Effective area (surface normal to the incident radiation)
 - Surface reflectivity
 - Luminosity of the Sun
 - Distance to the Sun
- GPS satellites oriented so that the “Y-axis” is perpendicular to the direction of the Sun (solar sensors)
- For satellites in the Earth shadow region (eclipsing), the solar radiation pressure is zero.
- For precise orbit determination, the shadow region must be carefully determined using the relative positions of the Sun, Earth, and the satellites.

Terminology

Reflectivity (ν) – the proportion of radiation incident on a surface that is reflected, the reflected radiation being separated into diffuse (scattered) and specular (beamed) components.

Specularity (μ) – the proportion of reflected radiation that is reflected specularly. Specular reflection implies that the surface behaves like a perfect mirror.

Y-bias – a force acting along the spacecraft BFS Y-axis and believed to derive from NCF effects. A likely mechanism for the Y-bias is due to non-orthogonality of the solar panels with respect to the solar photon flux, as a result of attitude bias or variations. However, another possible contribution could come from heat dissipation effects of payload components.



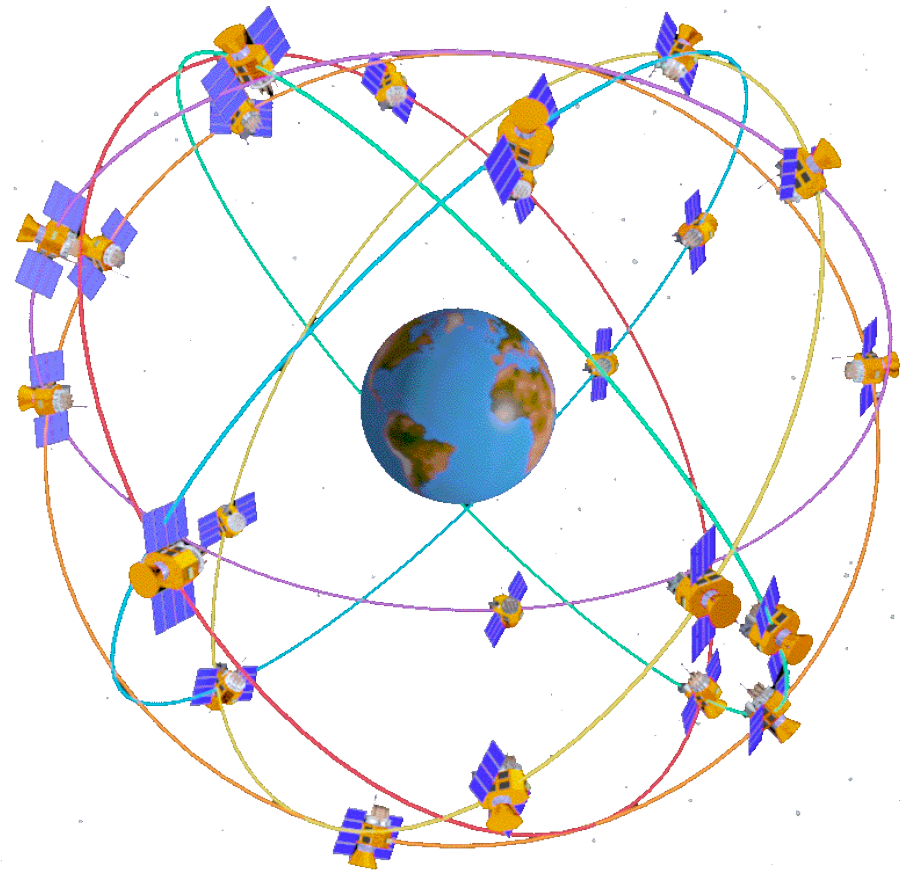
Reflected radiation from a spacecraft may be separated into diffuse and specular components. If a spacecraft's solar panels are not oriented precisely orthogonal to the photon flux, an anomalous bias force is generated along the spacecraft Y-axis.

Perturbed motion

Term	Acceleration (m/sec ²)	Perturbation (after 2 days)
Central	0.6	-
J ₂	5x10 ⁻⁵	14 km
Other gravity harmonics	3x10 ⁻⁷	0.1-1.5 km
Third body	5x10 ⁻⁶	1-3 km
Earth tides	10 ⁻⁹	0.5-1 m
Ocean tides	10 ⁻¹⁰	0-2 m
Drag	~0	-
Solar radiation	10 ⁻⁷	0.1-0.8 km
Albedo radiation	10 ⁻⁹	1-1.5 m

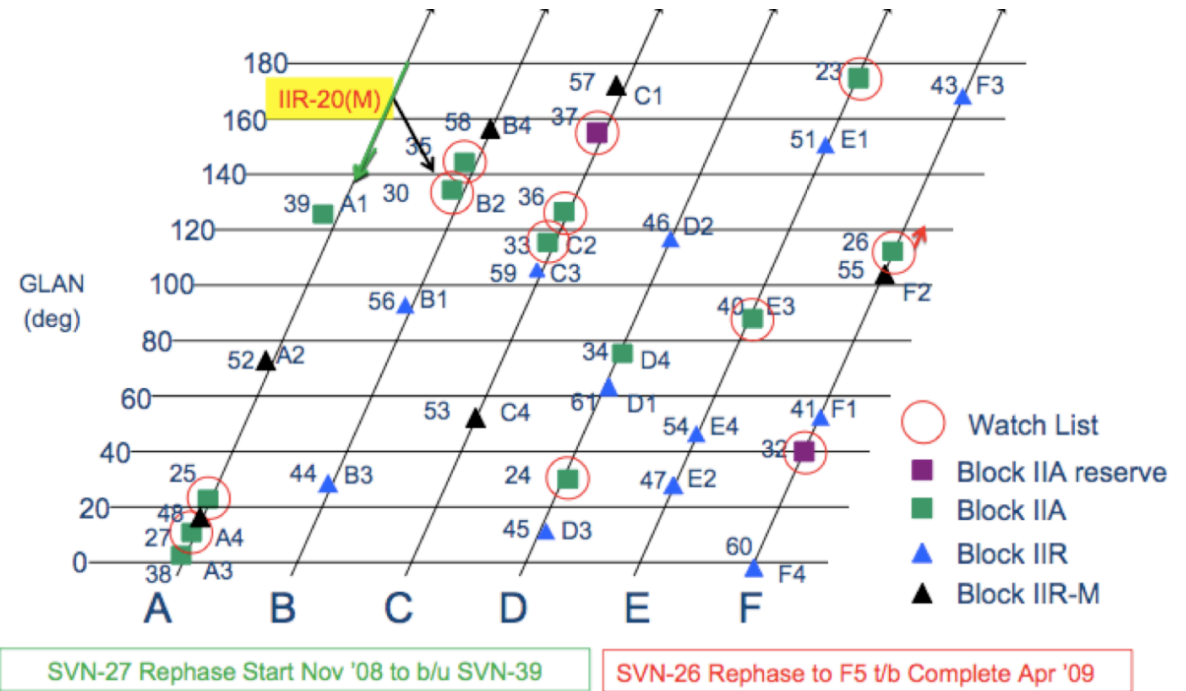
GPS orbits

- Orbit characteristics:
 - Semi-major axis = 26,400 km
 - Period = 12 sidereal hour
 - 6 orbital planes
 - Inclination = 55.5 degrees (except old block I sats = 63 deg., but all dead)
 - Eccentricity nearly 0 (largest 0.02) => quasi-circular orbits
- Full constellation = 24 satellites, completed March 9, 1994



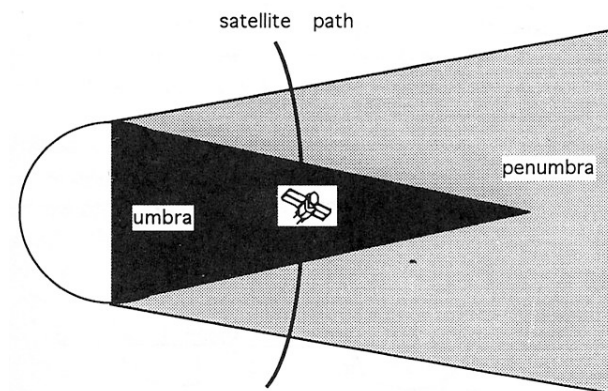
GPS Orbital Constellation

- 27 satellites (24 operational + 3 spares = nominal constellation)
- 6 evenly spaced orbital planes (A to F), inclination 55°
- 4-6 satellites per plane, spacing for optimized visibility
- Period = 12 sidereal hours (= 11h58mn “terrestrial” hours) => in a terrestrial frame, the constellation repeats every 23h56mn.



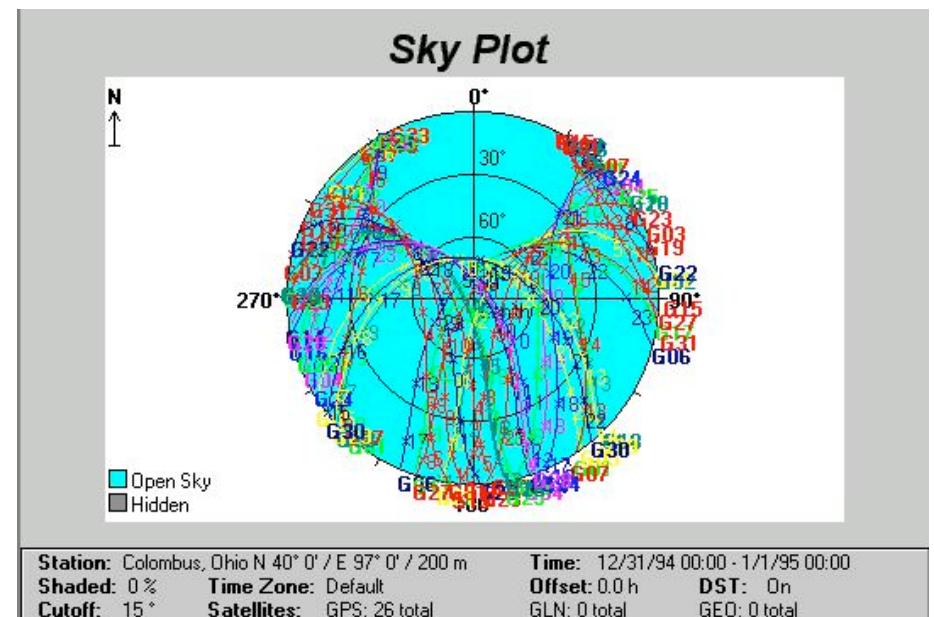
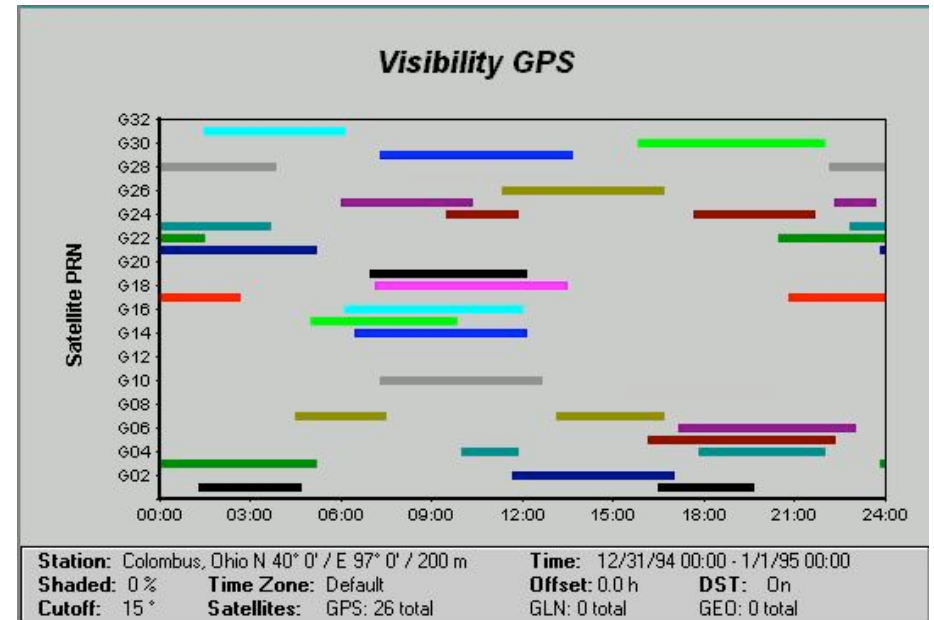
y-axis =longitude at which the satellite crosses the equator in the eastern hemisphere

- As Earth orbits around the Sun => eclipse periods (solar radiation pressure = 0, transition to shadow difficult to model, often simply edited out)



GPS satellite visibility

- Satellite visible up to 6 hours in a row (from rising to setting)
- In practice, 6-12 satellites are visible simultaneously, depending on:
 - Constellation geometry
 - User location
 - Elevation cut-off angle (chosen by the user)
- Problematic environments:
 - Forest
 - “urban canyons”
 - Mission planning may become necessary: determine best time of day to make measurements
- Site selection:
 - Must account for masks (minimal)
 - A! masks can grow (trees, houses)



GPS constellation

- Current status posted daily on <ftp://tycho.usno.navy.mil/pub/gps/gpstd.txt>
- Notice Advisories to NAVSTAR Users (NANUs) posted on: http://tycho.usno.navy.mil/gps_datafiles.html
- Or: <http://www.navcen.uscg.gov/navinfo/Gps/ActiveNanu.aspx>

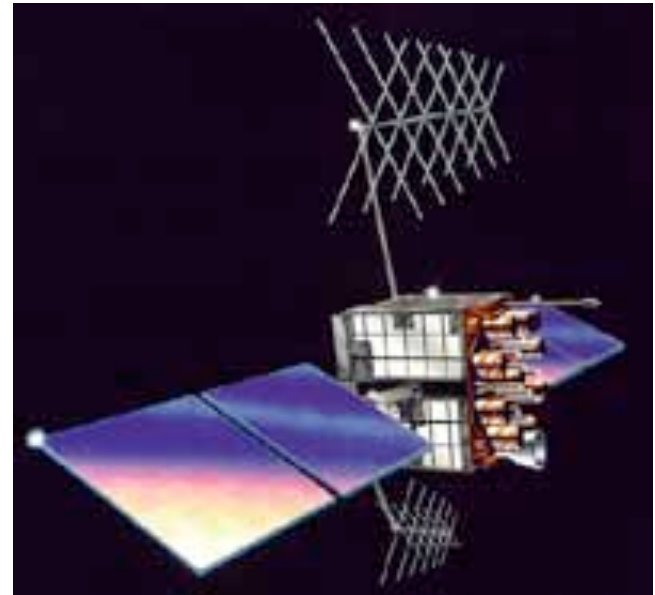
CURRENT BLOCK II/IIA/IIR/IIR-M SATELLITES

LAUNCH ORDER	PRN	SVN	LAUNCH DATE	FREQ STD	PLANE	US SPACE COMMAND **
*II-1		14	14 FEB 1989			19802
*II-2		13	10 JUN 1989			20061
*II-3		16	18 AUG 1989			20185
*II-4		19	21 OCT 1989			20302
*II-5		17	11 DEC 1989			20361
*II-6		18	24 JAN 1990			20452
*II-7		20	26 MAR 1990			20533
*II-8		21	02 AUG 1990			20724
*II-9		15	01 OCT 1990			20830
IIA-10	32	23	26 NOV 1990	Rb	E5	20959
IIA-11	24	24	04 JUL 1991	Cs	D5	21552
IIA-12	25	25	23 FEB 1992	Rb	A5	21890
*IIA-13		28	10 APR 1992			21930
IIA-14	26	26	07 JUL 1992	Rb	F5	22014
IIA-15	27	27	09 SEP 1992	Cs	A4	22108
*IIA-16		32	22 NOV 1992		F6	22231
*IIA-17		29	18 DEC 1992			22275
*IIA-18		22	03 FEB 1993			22446
*IIA-19		31	30 MAR 1993			22581
*IIA-20		37	13 MAY 1993			22657
IIA-21	09	39	26 JUN 1993	Cs	A1	22700
*IIA-22		35	30 AUG 1993	Rb	B5	22779
IIA-23	04	34	26 OCT 1993	Rb	D4	22877
IIA-24	06	36	10 MAR 1994	Rb	C5	23027
IIA-25	03	33	28 MAR 1996	Cs	C2	23833
IIA-26	10	40	16 JUL 1996	Cs	E3	23953
IIA-27	30	30	12 SEP 1996	Cs	B2	24320
IIA-28	08	38	06 NOV 1997	Cs	A3	25030
***IIR-1		42	17 JAN 1997			
IIR-2	13	43	23 JUL 1997	Rb	F3	24876
IIR-3	11	46	07 OCT 1999	Rb	D2	25933
IIR-4	20	51	11 MAY 2000	Rb	E1	26360
IIR-5	28	44	16 JUL 2000	Rb	B3	26407
IIR-6	14	41	10 NOV 2000	Rb	F1	26605
IIR-7	18	54	30 JAN 2001	Rb	E4	26690
IIR-8	16	56	29 JAN 2003	Rb	B1	27663
IIR-9	21	45	31 MAR 2003	Rb	D3	27704
IIR-10	22	47	21 DEC 2003	Rb	E2	28129
IIR-11	19	59	20 MAR 2004	Rb	C3	28190
IIR-12	23	60	23 JUN 2004	Rb	F4	28361
IIR-13	02	61	06 NOV 2004	Rb	D1	28474
IIR-14M	17	53	26 SEP 2005	Rb	C4	28874
IIR-15M	31	52	25 SEP 2006	Rb	A2	29486
IIR-16M	12	58	17 NOV 2006	Rb	B4	29601
IIR-17M	15	55	17 OCT 2007	Rb	F2	32260
IIR-18M	29	57	20 DEC 2007	Rb	C1	32384
IIR-19M	07	48	15 MAR 2008	Rb	A6	32711
IIR-20M	01	49	24 MAR 2009	Rb	B2	34661
IIR-21M	05	50	17 AUG 2009	Rb	E6	35752

* Satellite is no longer in service.
 ** US SPACE COMMAND, previously known as the NORAD object number; also referred to as the NASA Catalog number. Assigned at successful launch. Catalog numbers retrieved from SPACEWARN Bulletins: <http://nssdc.gsfc.nasa.gov/spacewarn/>
 *** Unsuccessful launch.

GPS satellites

- Solar powered
- S-Band (SGLS) communications for control and telemetry + UHF cross-link between spacecraft.
- Two L-Band navigation signals at 1575.42 MHz (L1) and 1227.60 MHz (L2).
- Each spacecraft carries 2 rubidium or 2 cesium clocks.
- Several generations of GPS satellites have been built and launched (next slide):
 - Different masses and phase center
 - Different capabilities



Block IIR satellite

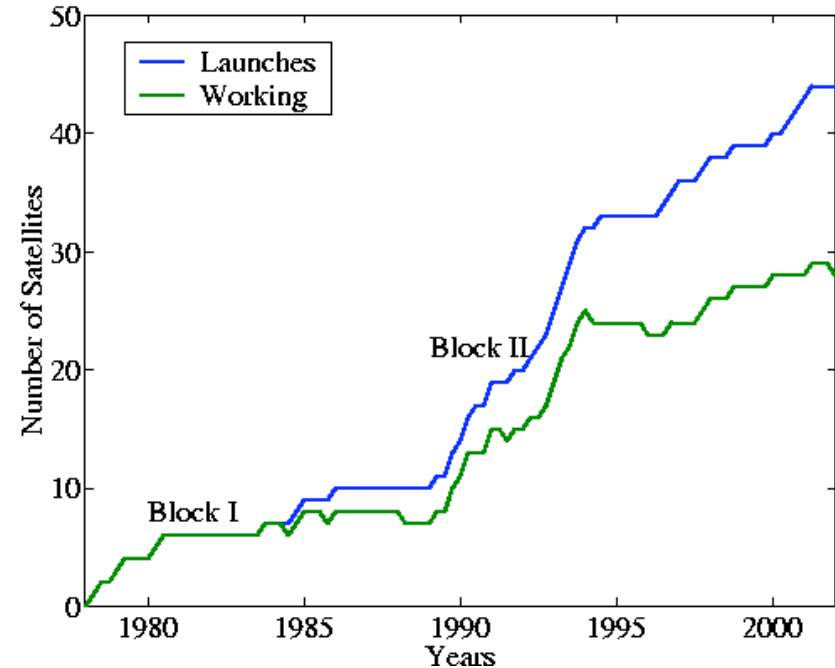


Dec. 20, 2007, launch

GPS satellites

- Block I: “proof-of-concept”, 1978 to 1985.
 - 11 satellites launched between 1978 and 1985 Life expectancy = 4.5 years, actual mean life = 7.1 years
 - Signal entirely accessible to civilian users
 - Last block I satellite died on Feb. 28, 1994
- Block II (II,IIA,IIR, IIR-M)
 - First launch 1989, latest launch December 20, 2007
 - Possibility to degrade the signal for civilian users (= selective availability)
- Next generation: Block III, 2010
 - Selective availability eliminated
 - Additional navigation signals
- Details on: http://www.spaceandtech.com/spacedata/constellations/navstar-gps_consum.shtml

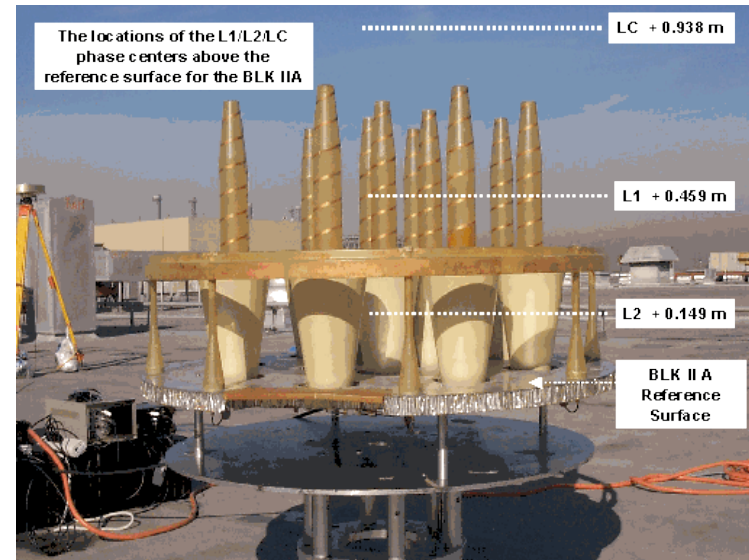
(Successful) GPS Satellite Launches



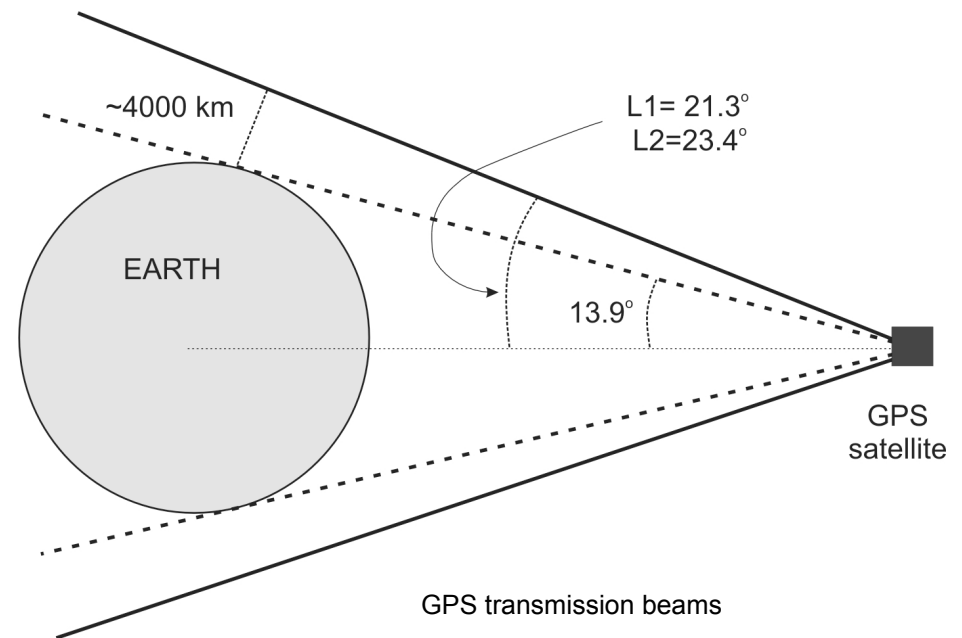
	Block I	Block II / IIA	Block IIR	Block IIF
Number	11	28	21	12
First launch	1978	1989	1997	2005
Mass (kg)	760	1660	2000	?
Power (W)	410	710	1100	2400
Design life (yr)	5	7.5	10	15
Cost	?	43 M\$	30M\$	28M\$
Contractor	Rockwell	Rockwell	Lockheed Martin	Rockwell

Satellite transmissions

- GPS satellites broadcast continuously on 2 frequencies in the L-band
 - 1575.42 MHz (L1)
 - 1227.60 MHz (L2)
- GPS antennas point their transmission antenna to the center of the Earth (controlled by solar sensors).
- Main beam = 21.4/23.4 (L1/L2) half width.
- Phase center of antenna does not coincide with center of gravity of satellite.



Transmission antenna of a block II-R GPS satellite



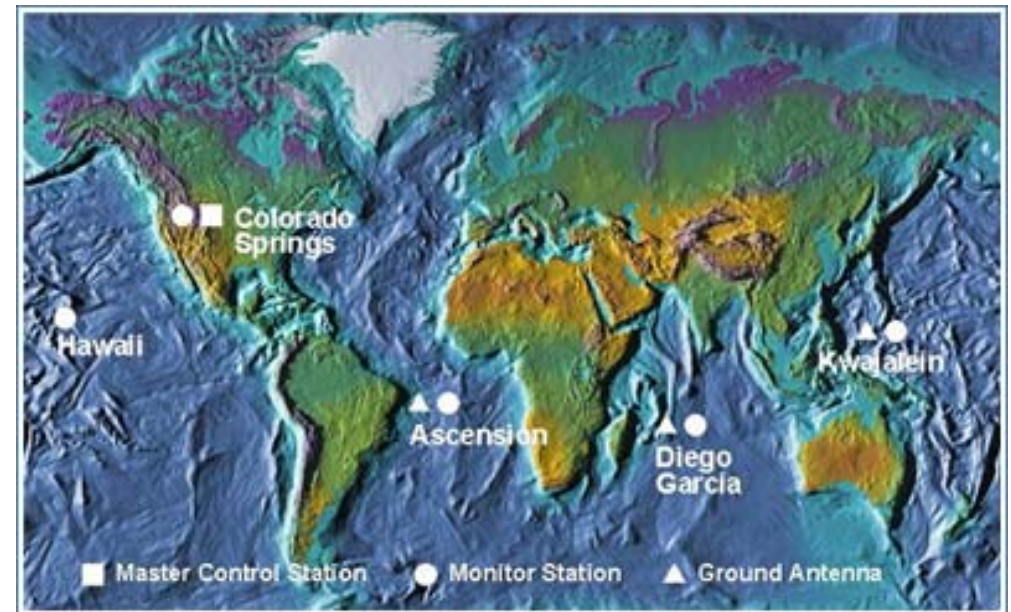
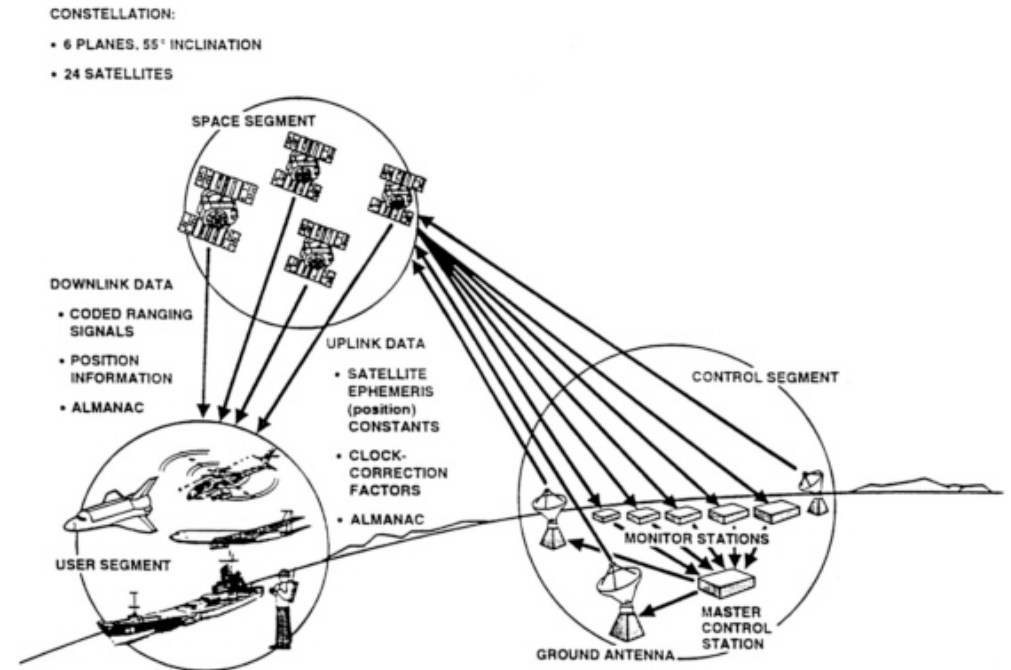
Satellite clocks

- Frequencies broadcast by GPS satellites are derived from a **fundamental frequency of 10.23 Mhz**
- Fundamental frequency provided by 2 or 4 atomic clocks (Ce/Rb)
 - Clocks run on GPS time = UTC not adjusted for leap seconds
 - Clock stability over 1 day = 10^{-13} (Rb) to 10^{-14} (Ce), ~ 1 ns/day
 - Clocks **synchronized between all satellites**
- Relativistic effects:
 - Clocks in orbit appear to run faster (38.3 microsec/day = 11.5 km/day!) => tuned at 10.22999999543 MHz before launching (g.)
 - Clocks speed is a function of orbit eccentricity (45 nsec = 14 m) => corrected at the data processing stage (s.):

$$\Delta t_R = -\frac{2}{c^2} \sqrt{a\mu} e \sin E$$

GPS control segment

- Monitor stations:
 - Monitor behavior of satellite orbit and clock, health of satellites
 - Uploads data to satellites according to orders from Master station.
- Master station:
 - Located at Falcon Air Force Base in Colorado Springs, Colorado
 - Calculates position and clock errors for each individual satellite based on information received from the monitor stations
 - Orders appropriate ground antennas to relay information back to satellites
 - Order maneuvers when necessary
 - Ensure clock synchronization = defines GPS time
- Computes and uploads **broadcast ephemerides** into the satellites



The GPS control segment

GPS broadcast ephemeris

- Distributed to users as part of the GPS signal in the navigation message included in the signal sent by the satellites.
- Following parameters are included:
 - Keplerian elements with periodic terms added to account for solar radiation and gravity perturbations.
 - Periodic terms are added for argument of perigee, geocentric distance and inclination.
 - Reference system is WGS84.
- Navigation message:
 - Updated every 2 hours
 - Considered valid from 2 hours before Time of Ephemeris (TOE) until 2 hours after TOE
 - Decoded by all GPS receivers from GPS signal
 - Distributed in ASCII format in *Receiver Independent Exchange* format (RINEX): [4-char][Day of year] [Session].[yy]n (e.g. brdc0120.02n)

svprn	satellite PRN number
m_0	mean anomaly
t_{oe}	time of ephemeris
\sqrt{a}	sqrt(semi-major axis)
Δn	variation of mean angular velocity
e	eccentricity
ω_0	argument of perigee
i_0	inclination
\dot{i}	rate of inclination
Ω_0	right ascension
$\dot{\Omega}$	rate of right ascension
$C_{wc} C_{ws} C_{rc} C_{rs} C_{ic}$ C_{is}	correction coefficients

GPS broadcast ephemeris

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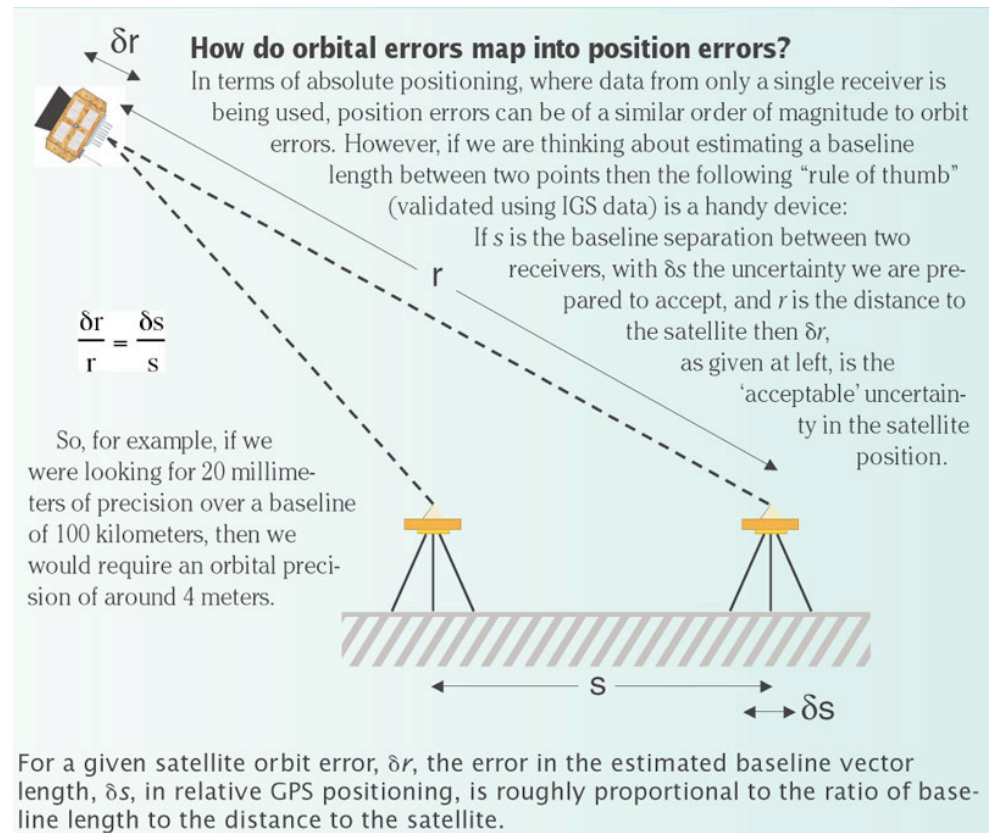
2          NAVIGATION DATA          RINEX VERSION / TYPE
comb_nav.pl  SOPAC      Fri Jan 11 04:00:16 GMT 2002 PGM / RUN BY / DATE
          BROADCAST EPHEMERIS FILE          COMMENT
          COMMENT
          SOPAC - Scripps Orbit and Permanent Array Center          COMMENT
          IGPP - Institute of Geophysics and Planetary Physics          COMMENT
          SIO - Scripps Institution of Oceanography          COMMENT
          UCSD - University of California, San Diego          COMMENT
          email: archive@lox.ucsd.edu          COMMENT
          ftp://lox.ucsd.edu          COMMENT
          http://lox.ucsd.edu          COMMENT
          COMMENT
          END OF HEADER
1 02 1 10 0 0 0.0 2.108854241669D-04 1.591615728103D-12 0.000000000000D+00
  1.740000000000D+02-6.625000000000D+01 3.994452099249D-09 2.453913345123D+00
-3.479421138763D-06 5.274268332869D-03 1.066364347935D-05 5.153708732605D+03
  3.456000000000D+05 1.378357410431D-07-2.987566298300D-01-2.235174179077D-08
  9.676350812908D-01 1.789375000000D+02-1.727933015620D+00-7.573886911362D-09
  3.507288949806D-10 0.000000000000D+00 1.148000000000D+03 0.000000000000D+00
  2.800000000000D+00 0.000000000000D+00-3.259629011154D-09 4.300000000000D+02
  3.455400000000D+05
1 02 1 10 2 0 0.0 2.108966000378D-04 1.591615728103D-12 0.000000000000D+00
  1.750000000000D+02-7.146875000000D+01 3.928377918423D-09-2.779033653221D+00
-3.810971975327D-06 5.274182534777D-03 1.071207225323D-05 5.153708749771D+03
  3.528000000000D+05 4.284083843231D-08-2.988106363767D-01 1.862645149231D-09
  9.676374409777D-01 1.748125000000D+02-1.728015465683D+00-7.532456614195D-09
  3.014411276615D-10 0.000000000000D+00 1.148000000000D+03 0.000000000000D+00
  4.000000000000D+00 0.000000000000D+00-3.259629011154D-09 4.310000000000D+02
  3.456000000000D+05
1 02 1 10 4 0 0.0 2.109077759087D-04 1.591615728103D-12 0.000000000000D+00
  1.760000000000D+02-6.781250000000D+01 3.973379792931D-09-1.728982466237D+00
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  3.600000000000D+05 1.192092895508D-07-2.988646707189D-01 1.043081283569D-07
  9.676391291852D-01 1.698437500000D+02-1.727911795993D+00-7.616031523997D-09
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  4.000000000000D+00 0.000000000000D+00-3.259629011154D-09 4.320000000000D+02
  3.528000000000D+05
1 02 1 10 6 0 0.0 2.109189517796D-04 1.591615728103D-12 0.000000000000D+00
  1.770000000000D+02-6.131250000000D+01 4.097670684432D-09-6.787591172017D-01
-3.200024366379D-06 5.274690338410D-03 1.081638038158D-05 5.153708938599D+03
  3.672000000000D+05-1.154839992523D-07-2.989205995400D-01 6.146728992462D-08
  9.676398972172D-01 1.711250000000D+02-1.727978344137D+00-7.836397845996D-09
  2.517962026082D-10 1.000000000000D+00 1.148000000000D+03 0.000000000000D+00
  4.000000000000D+00 0.000000000000D+00-3.259629011154D-09 4.330000000000D+02
  3.646380000000D+05
...etc

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TABLE A4 NAVIGATION MESSAGE FILE - DATA RECORD DESCRIPTION		
OBS. RECORD	DESCRIPTION	FORMAT
PRN / EPOCH / SV CLK	- Satellite PRN number - Epoch: Toc - Time of Clock year (2 digits) month day hour minute second - SV clock bias (seconds) - SV clock drift (sec/sec) - SV clock drift rate (sec/sec2)	I2, 5I3, F5.1, 3D19.12
BROADCAST ORBIT - 1	- IODE Issue of Data, Ephemeris - Crs (meters) - Delta n (radians/sec) - M0 (radians)	3X,4D19.12
BROADCAST ORBIT - 2	- Cuc (radians) - e Eccentricity - Cus (radians) - sqrt(A) (sqrt(m))	3X,4D19.12
BROADCAST ORBIT - 3	- Toe Time of Ephemeris (sec of GPS week) - Cic (radians) - OMEGA (radians) - CIS (radians)	3X,4D19.12
BROADCAST ORBIT - 4	- i0 (radians) - Crc (meters) - omega (radians) - OMEGA DOT (radians/sec)	3X,4D19.12
BROADCAST ORBIT - 5	- IDOT (radians/sec) - Codes on L2 channel - GPS Week # (to go with TOE) - L2 P data flag	3X,4D19.12
BROADCAST ORBIT - 6	- SV accuracy (meters) - SV health (MSB only) - TGD (seconds) - IODC Issue of Data, Clock	3X,4D19.12
BROADCAST ORBIT - 7	- Transmission time of message (sec of GPS week, derived e.g. from Z-count in Hand Over Word (HOW)) - spare - spare - spare	3X,4D19.12

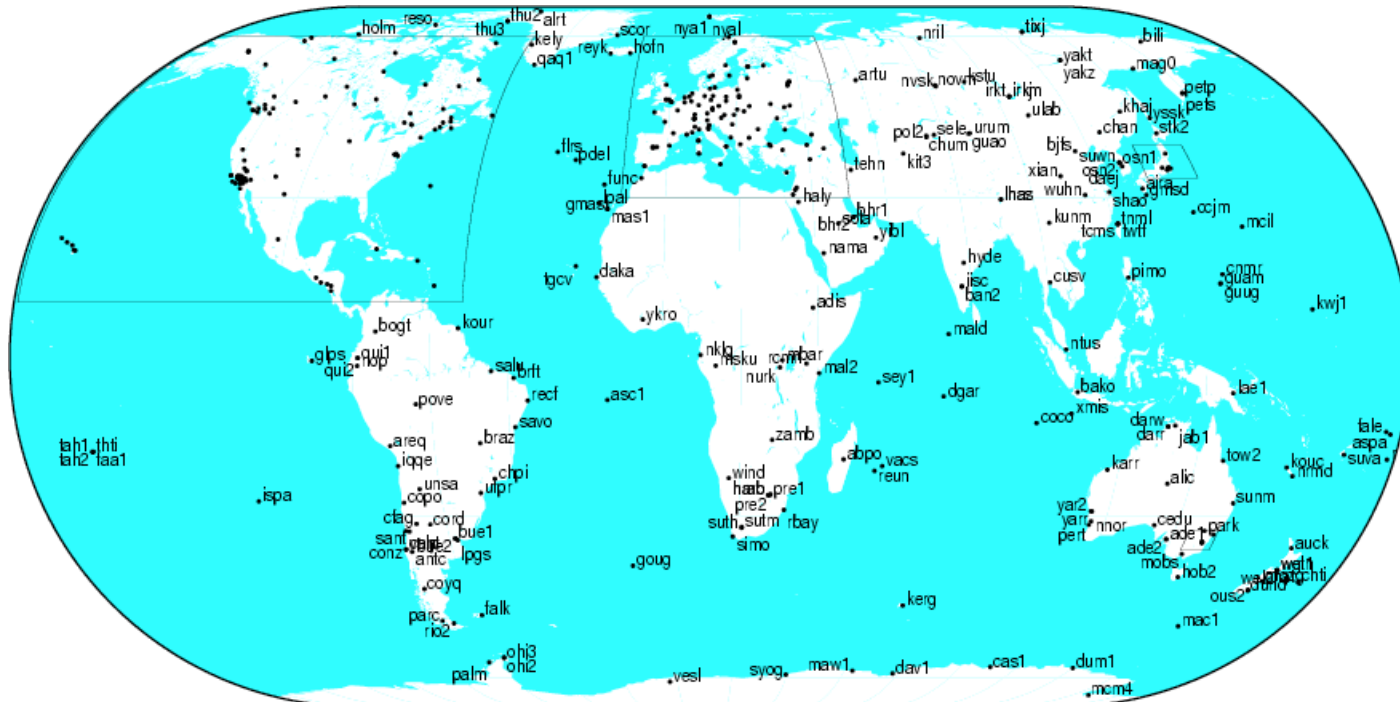
GPS broadcast ephemeris

- Accuracy of broadcast ephemeris:
 - ~ 10 m
 - Can be degraded by the DoD to 300 m
 - $\delta s/s = \delta r/r \Rightarrow$ if $\delta r = 200$ m ($r = 20\,000$ km):
 - $s = 100$ km $\Rightarrow \delta r = 1$ m, not sufficient for geophysical applications
 - $s = 1$ km $\Rightarrow \delta r = 1$ cm, sufficient for surveying
- Broadcast ephemerides are not accurate enough for most geophysical applications.
- Requirements for geophysical applications (mm – cm level):
 - Accurate orbits: e.g. 10 cm orbit error \Rightarrow 0.5 mm error on a 100 km baseline
 - Independent from the DoD



IGS: The International GNSS Service for Geodynamics

- International service of the IAG (International Association of Geodesy)
- Coordinates data archiving and processing of a global control network of >350 dual-frequency permanent GPS stations
- Test campaign in 1992, routine operations since 1994
- Provides precise GPS products, in particular satellite orbits

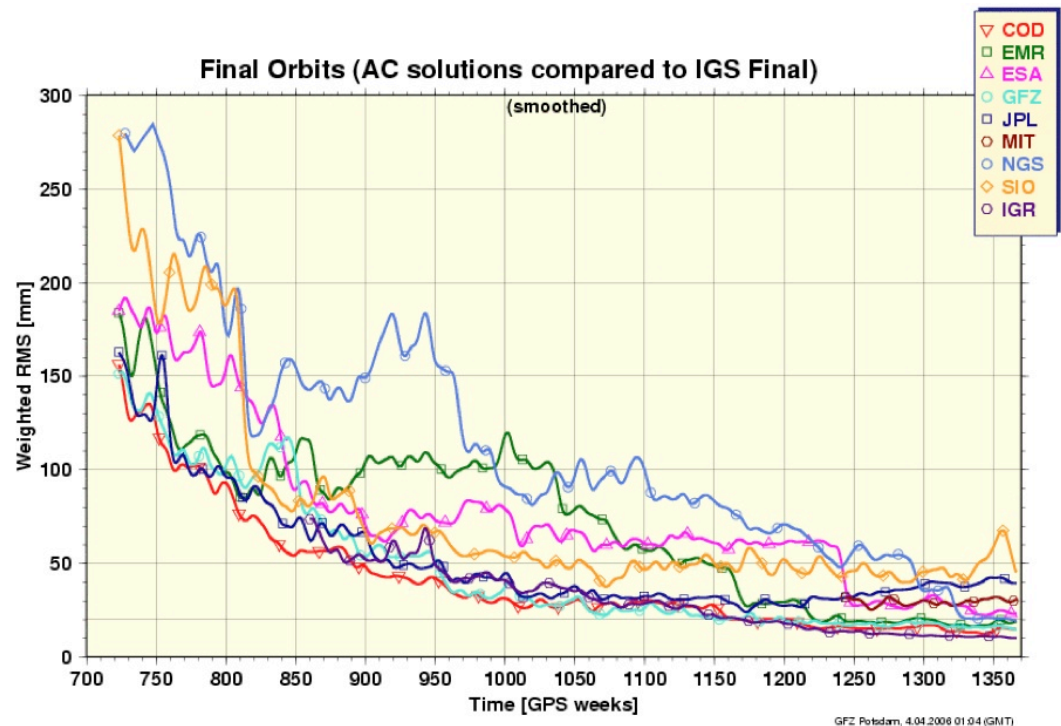


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Map of IGS station distribution - <http://igsceb.jpl.nasa.gov/>

IGS orbits

- Core network of globally distributed, high-quality, continuous GPS stations
- Data processed by IGS analysis centers
- Analysis center coordinator produces weighted average = final IGS orbit
- Process takes 2 weeks (to ensure best station distribution and solution quality)
- IGS also provides satellite clock corrections
- Other products:
 - Rapid
 - Predicted



Graph courtesy Analysis Coordinator G. Gendt, GFZ Potsdam

Orbits Type	Accuracy/clock accuracy	Latency	Updates	Sample interval
Broadcast	~260 cm/~7 ns	Real-time		daily
Final	< 5 cm/0.1 ns	14 days	Weekly	15 min
Rapid	5 cm/0.2 ns	17 hours	Daily	15 min
Predicted (ultra-rapid)	~10 cm/~7 ns	Real-time	Twice daily	15 min

Orbit comparison: IGS - broadcast

